## GEOTECHNICAL INSTRUMENTATION: Ensuring Safety & Stability of ERSS

BY THET LINN SEPT, 2024

## Content:

## Over view

- Type of wall
- Design Consideration & Failure modes
- Objective in Instrumentations and Types
- Main Application of JGP in Deep Excavation
- Authority Guideline
- How to Access/ Interpret Instrumentation & Monitoring Data & Report





(a). Before collapse

The collapse was caused by

- poorly designed <u>strut-waler support</u> system,
- Clack of monitoring and proper management of data caused by human error,
- organisational failures



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(b).After collapse

# NICOLL HIGHWAY COLLAPSE 20 April 2004

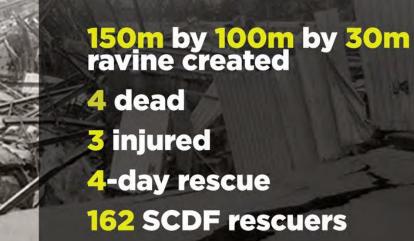
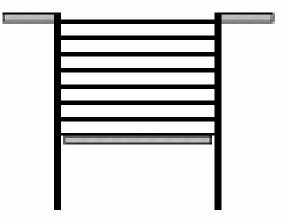


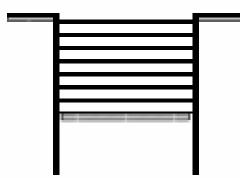
Image: National Library Board Singapore

Inexperienced personnel had been appointed to monitor the safety of the retaining wall system

- higher standard of reliability and accuracy in monitoring data



# A robust design is the most important step towards a successful excavation.



## A poor design brings...

Headache

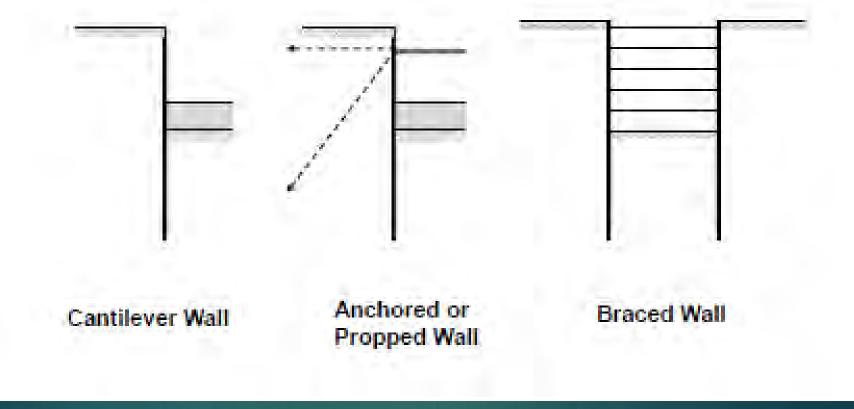
Trouble

## Disaster III

The end result is cost over-run and time delay!

## TYPE OF WALL FOR DEEP EXCAVATION

## **Types of Retaining Walls for Excavation**



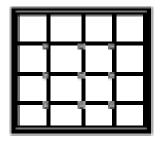
## WHAT IS A BRACED CUT?

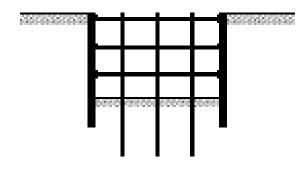
An excavation supported by suitable bracing system are called braced cut. These excavation support systems are used to,

- Minimized the excavation area,
- Keep the sides of deep excavations stable, and Ensure that movements of soil
- Will not cause damage to neighboring structures or utilities

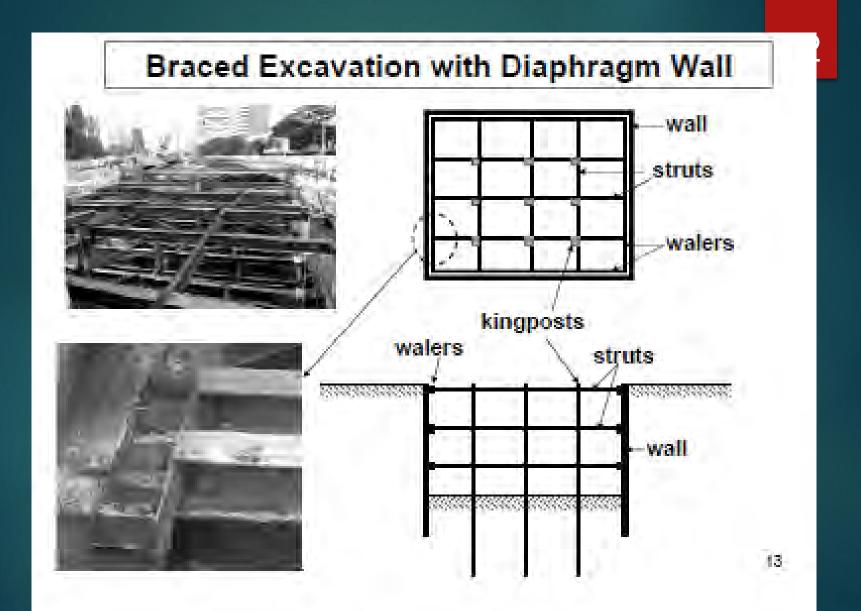
in the surrounding ground.

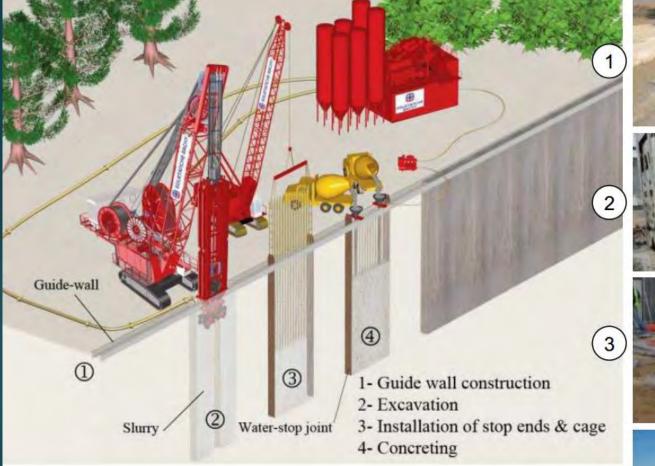
## Wall Types of Deep Excavations





- Diaphragm Wall
- Sheetpile Wall
- Bored Pile Wall
- Soldier Pile Wall
- DCM or Grout Mixed Pile Wall







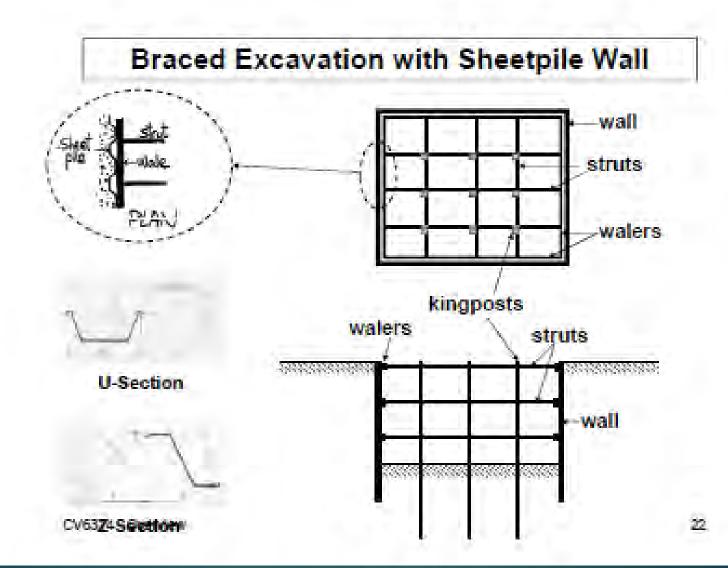




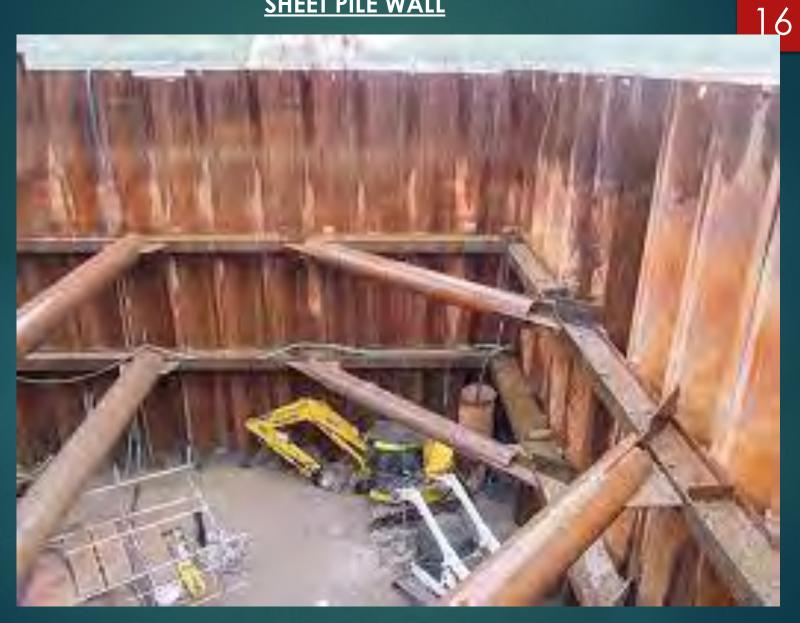


## DIAPHRAM WALL CONSTRUCTION (5:30 MINUTES)

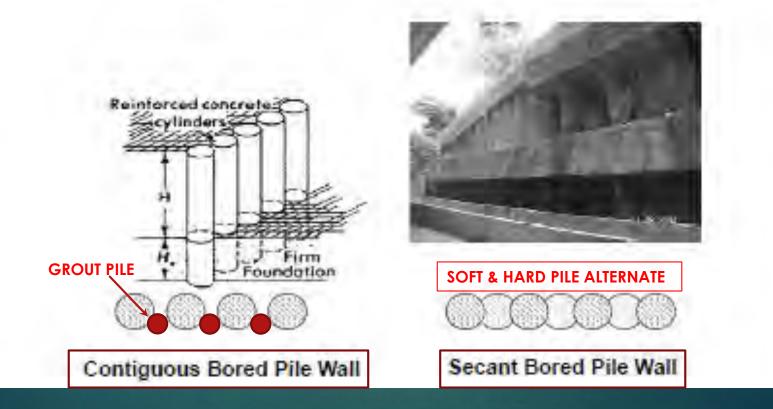


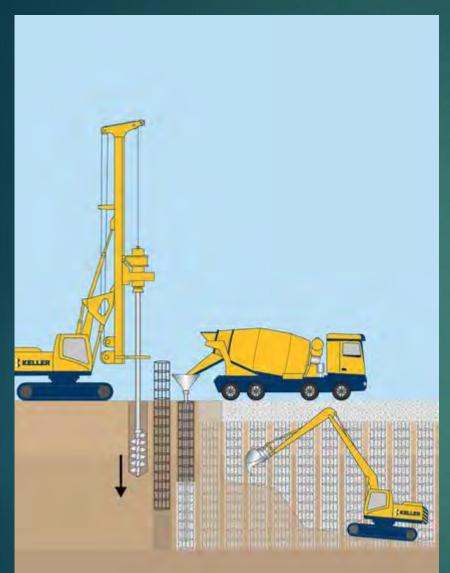


## SHEET PILE WALL



## **Bored Pile Walls**





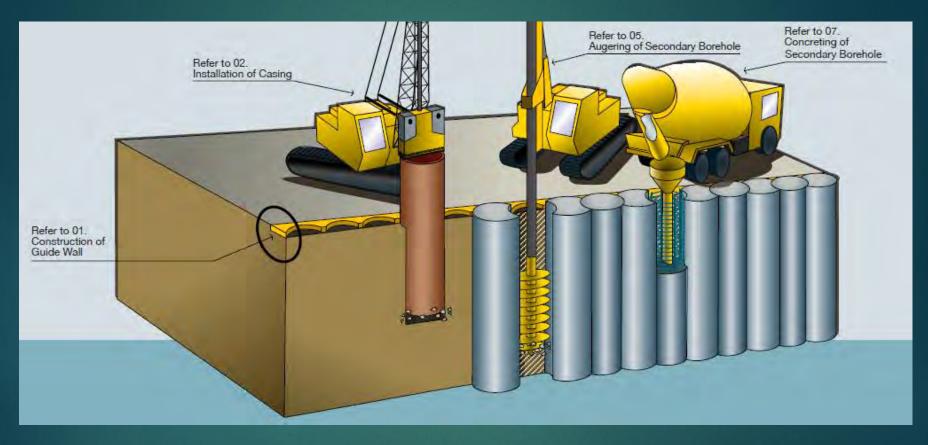
## 18

## CONTINUOUS BORED PILE WALL



## 19

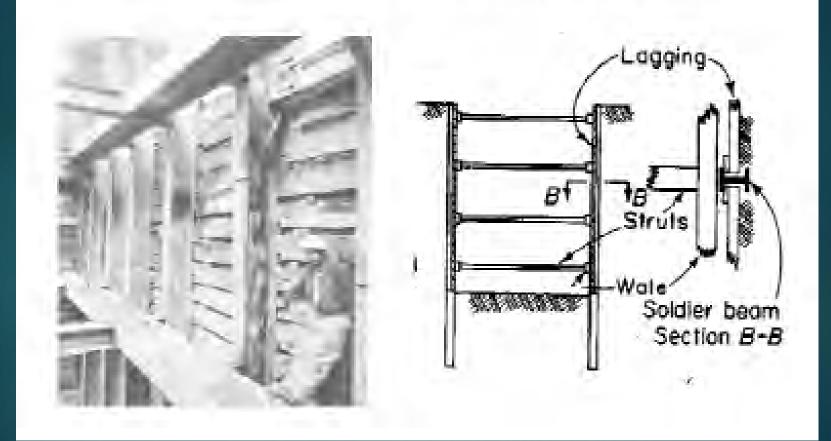
#### **SECANT PILE WALL**



## SECANT PILE WALL CONSTRUCTION (2:45 MINUTES)



## **Braced Excavation with Soldier Pile Wall**

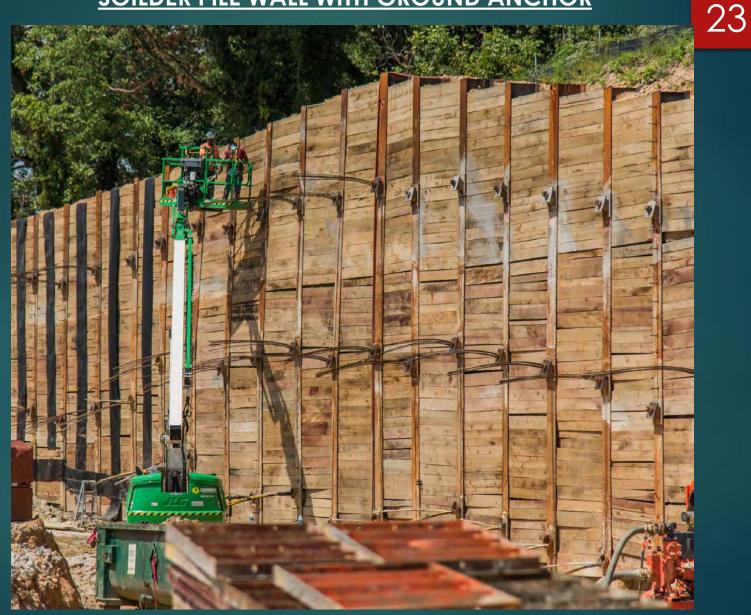


21

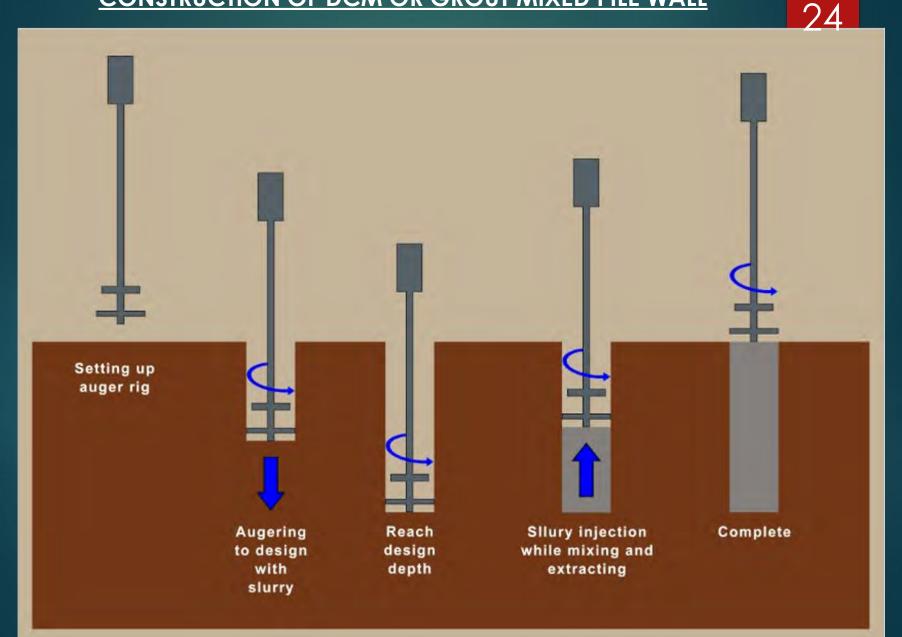
## SOLDIER PILE CONSTRUCTION (0:27 MINUTE)



#### SOILDER PILE WALL WITH GROUND ANCHOR



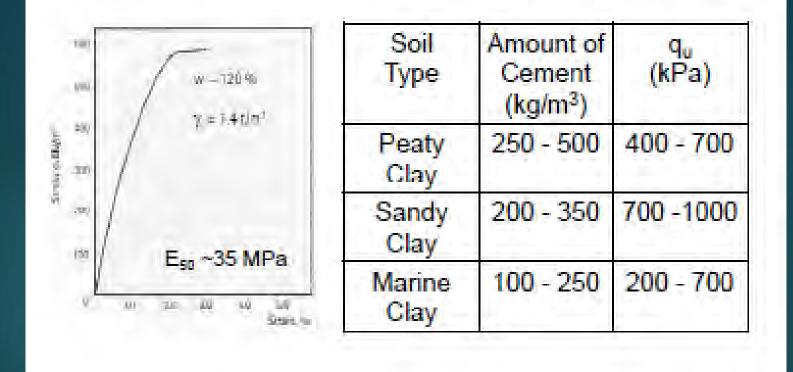
#### CONSTRUCTION OF DCM OR GROUT MIXED PILE WALL



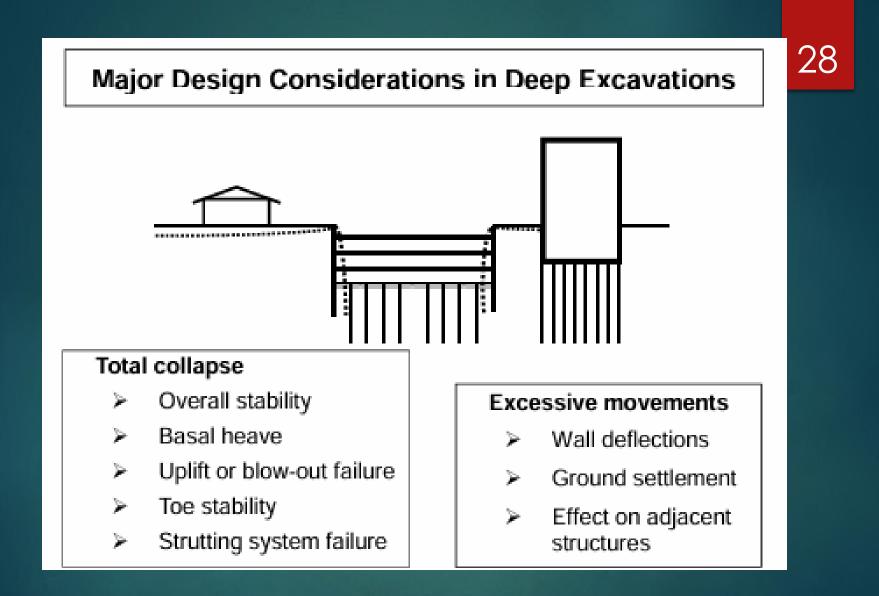


## 26

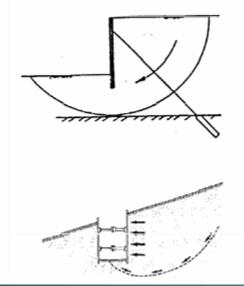
#### Properties of DCM or Grout Mixed Pile Wall



# DESIGN CONSIDERATION & FAILURE MODES



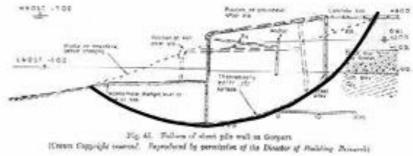
Overall Stability



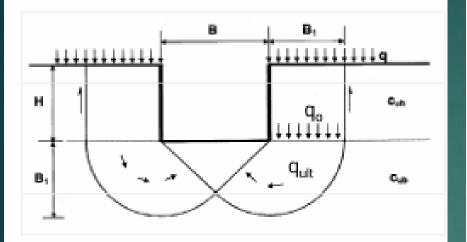


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#### **Basal Heave Stability**



When  $q_o > q_{ult}$ , failure in imminent.

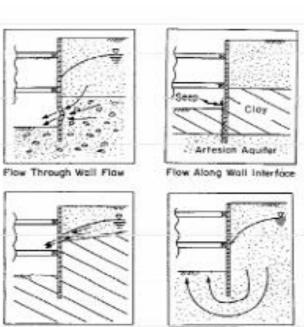
#### Lifting of Kingpost due to Bottom Heave



## Basal Heave Failure due to Stockpiling



#### Piping & Loss of Fines

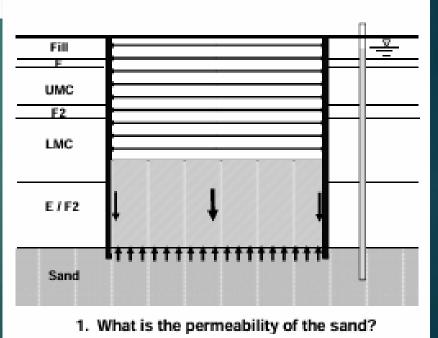


Flow From Perched Woter

Flow Benedth Woll

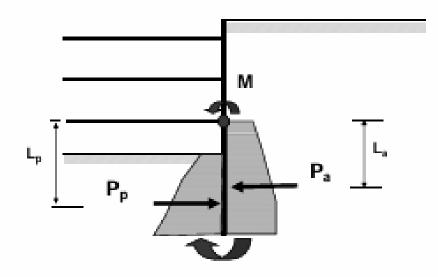
31

#### Uplift Instability or Blowout Failure



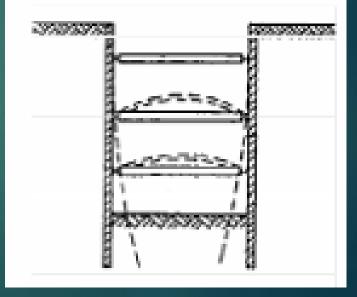
14 - Overview 2. Is there a free supply of water?

## **Toe Kick-out Stability**





## Strut Failure

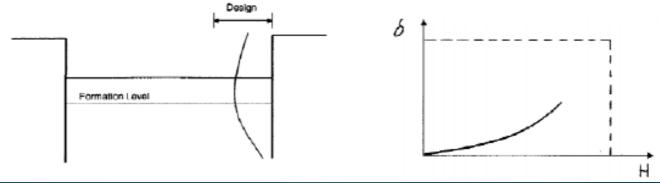


## Objective in Instrumentations & Type of Instruments/ Sensors

## **Objectives in Instrumentation**

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- To check whether the retaining wall system is in danger of impending failure.
- To check whether the performance criteria set forth in the specifications are met.
- 3. To facilitate the implementation of the Observational Method.
- To check the effectiveness of any preventive and remedial measures.
- 5. To protect against any unwarranted claims.



Wall Deflections :	In-wall inclinometers In-soil inclinometers Surveying points on wall top
Strut Forces :	Load cells
	Vibrating wire strain gauges
	Thermometers
Ground Settlements :	Surveying points
	Settlement plates
Movements at	
Surrounding Buildings :	Surveying points for vertical and horizontal movements
	Tilt plates
	Crack meters
Groundwater Level :	Water standpipes
Others : wall bending moment; excess pore pressure; bottom heave; tunnel movements and vibration	



#### In-soil Inclinometer



#### In-wall Inclinometer



#### In-Soil Inclinometers

- o Measure soil movements during:
  - (i) wall construction
  - (ii) jet grouting
  - (iii) excavation
  - (iv) basement slab construction

o The tip should be anchored into the hard stratum,

It should be located within 2 m from the wall.

The A-axis should be set perpendicular to the wall.

In most cases, use resultants from the A and B axes.

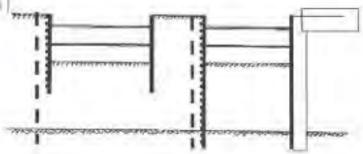
In-Wall Inclinometers ....

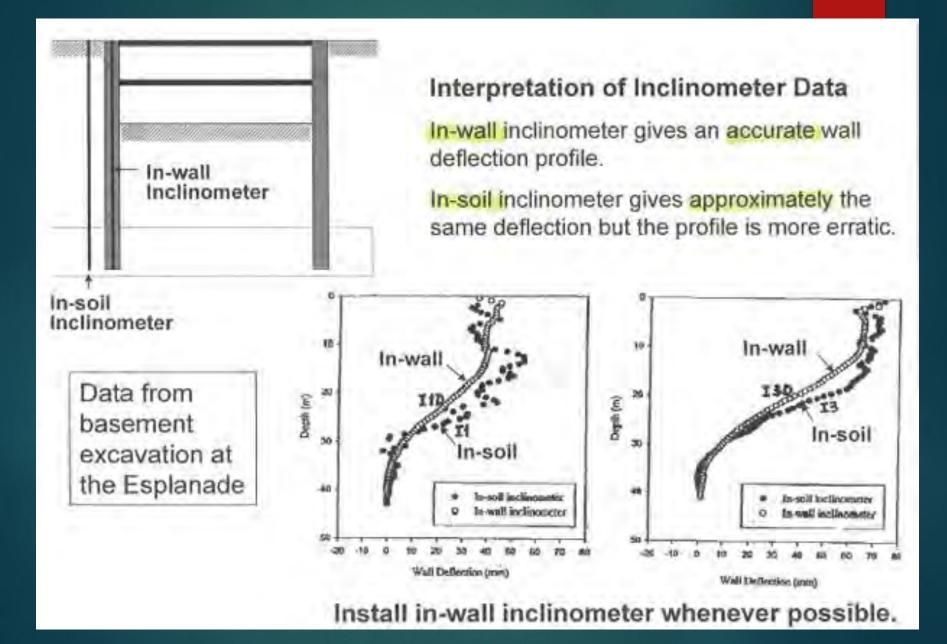
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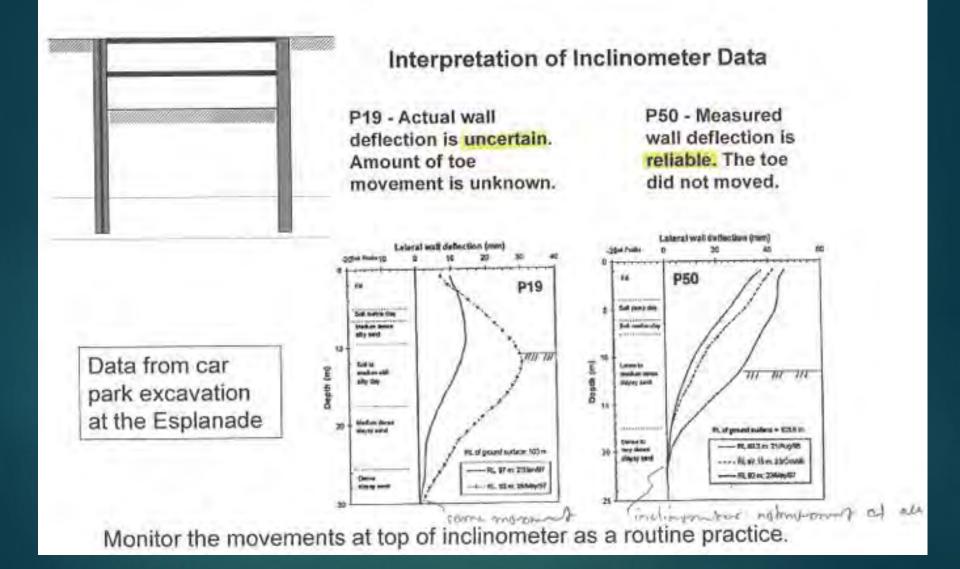
- Measure soil movements during:
  - (i) jet grouting
  - (ii) excavation
- Indirect measurement of bending moment in wall
- The A-axis should be set perpendicular to the wall. Use resultants from the A and B axes to compute wall movements.

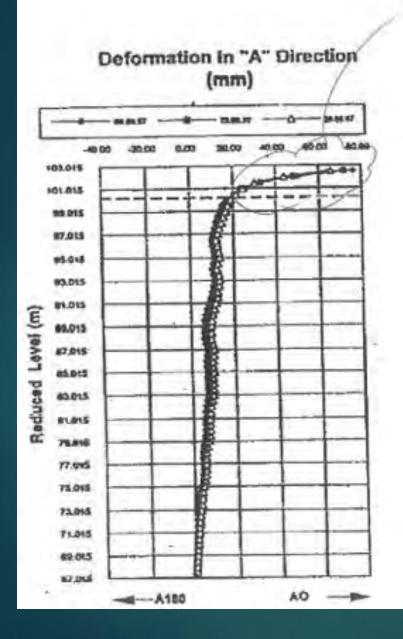
# In-Soil vs In-Wall Inclinometers

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## Interpretation of Inclinometer Data

Don't be alarmed by the deflection near the top of inclinometer. It gets disturbed easily during construction.



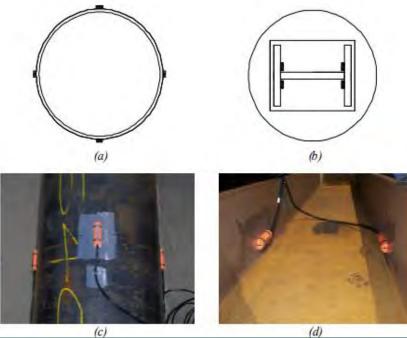


Need Proper protection!

# Load Cell

# Strain Gauge





(c)

# **Building & Ground Settlement Marker**





# Tilt Plate & Portable Tilt-meter





# Paper Prism







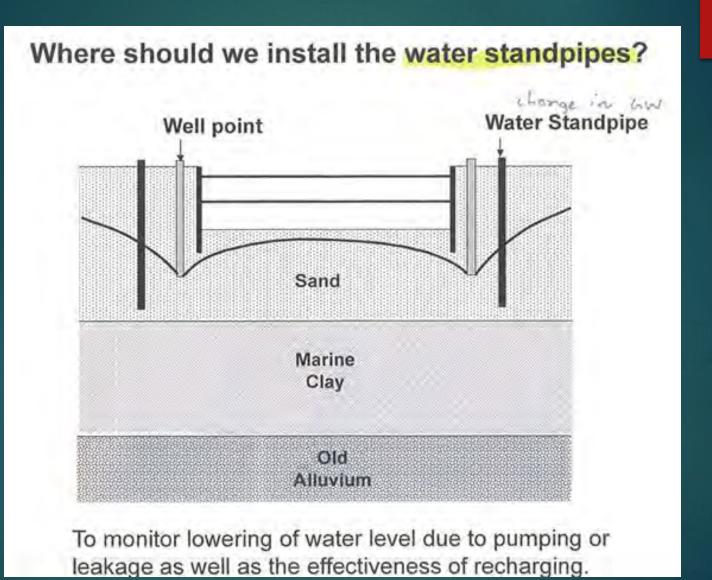
# **Cracked Meter**



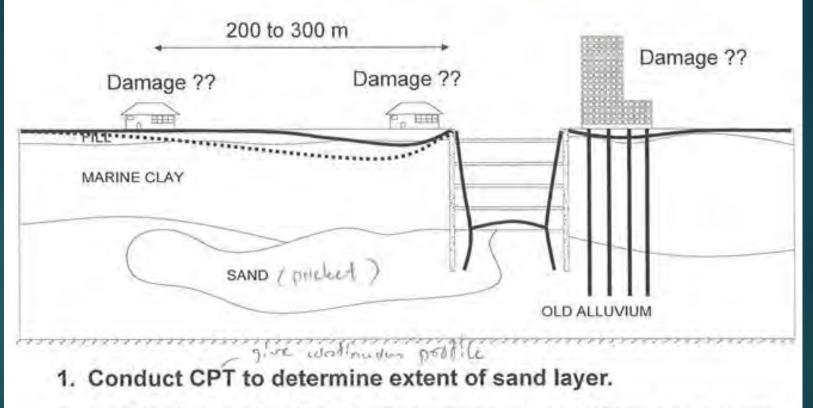
# 46

## Vibration Meter





## Where should we install the piezometers?



2. Conduct pumping test to check connectivity of the sand layer.

The water level inside the standpipes simply represents the level of the free groundwater table,

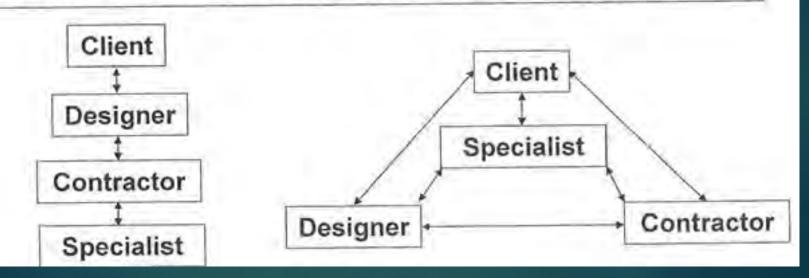
The water level inside the piezometers represents the pore water pressure at the depth of the piezometer tip, ...

# What is the contractual arrangement?

The instrumentation specialist (IS) should be employed directly by the client/developer. They should protect the client's interest.

This arrangement improves the communication between the IS and client, designer and contractor.

>If the contractor is IS's pay master, there may be a conflict of interest. There are known incidences of foul plays.



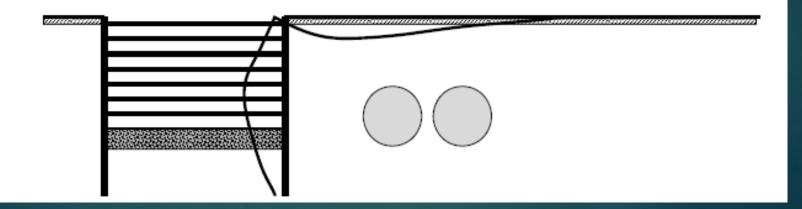
# Instrumentation

- 1. Don't skim on instrumentation. Penny wise but dollar foolish!
- 1. Engage a *reputable* company to install & monitor.
- 2. Engage a *qualified* engineer to review the data.
- 3. Designer should be one of the key players.
- 4. Review the data diligently.
- 5. Investigate causes of any sudden increases.
- 6. Add more instruments whenever necessary.
- The instrumentation specialist should be employed directly by the client and not the contractor.

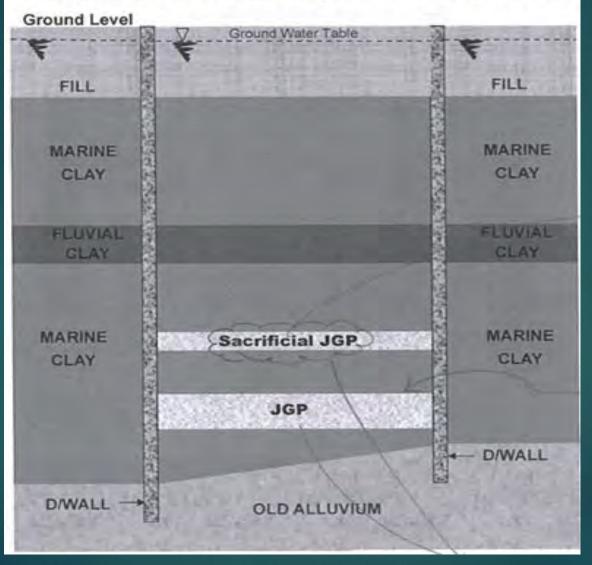
# Main Application of JGP in Deep Excavation

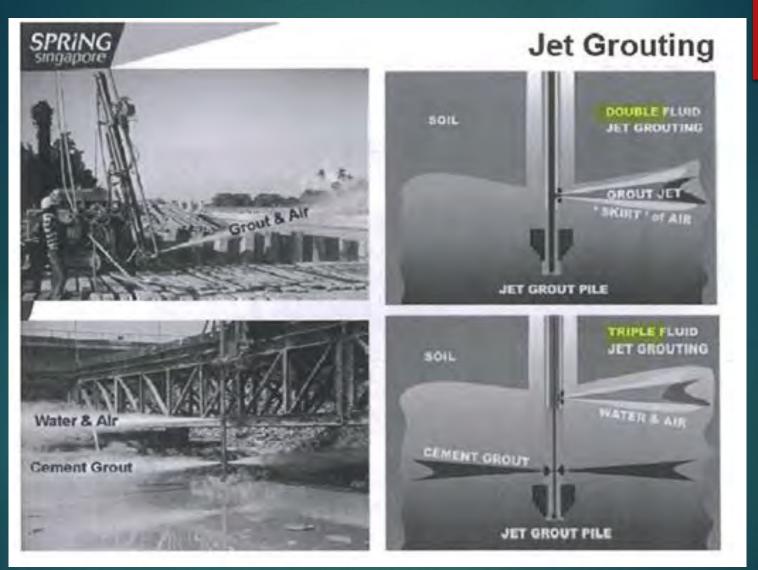
# Main applications of JGP in deep excavation are:

- 1. To reduce wall deflection & ground settlement
- 2. To minimize CST & MRT tunnel movements
- 3. To improve basal heave stability
- 4. To improve toe kick-in stability
- 5. To control seepage



#### **Completed JGP Slabs prior to Excavation**

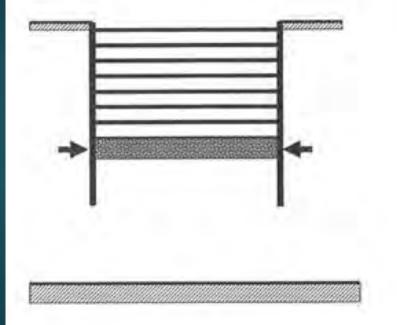




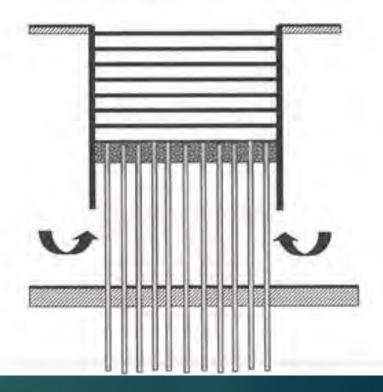
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# How does it work?

It acts as a compression member to reduce wall deflection.



In addition, it can also act as an **anchored slab** to minimize bottom heave.



# GUIDELINE FROM AUTHORITY?

# Submission Requirements for Earth Retaining or Stabilizing Structures for High Rise Buildings with Basement Construction

- 1. Deep excavation analysis and design
- 2. Instrumentation and monitoring system
- 3. Calculation of ERSS design
- 4. Submission Document Check-List
- 5. Presentation
- 6. Geotechnical Impact Assessment (GIA)
- Letter from YCDC (to be attached)



#### GEOTECHNICAL DESIGN

#### Basement Construction:

#### General Requirements for Excavation and Lateral Support (ELS)

- ELS plans submission document shall include the geotechnical assessment, geotechnical details and calculations, site investigation reports.
- Designer shall prepare and sign the plans and structural design as well as the structural assessment report of the effects of the excavation and dewatering on adjoining structures.
- ELS design report shall explain the references for recognized specifications and code of practice for design calculation.
- Construction methodology shall explain, for example, detail excavation and support installation sequence and then removal of temporary support, construction of permanent structure for each stage.
- 5. Designer shall prepare the impact assessment of surrounding building and facilities, monitoring plan and instrumentation. The impact assessment shall include hydrological assessment including surface and subsurface ground water flow, ground movement during and/after construction, vibration due to construction and mitigation of impacts on surrounding buildings and facilities.
- The followings shall be included in detail drawings of basement:
  - a) Detail drawings of all structural elements, joint connection, reinforcement and technical notes.
  - b) Detail site layout plan with adjacent buildings and bored hole location.
  - c) The construction structural details of the lateral support system, including detailing of the structural supports (struts, anchorage etc.) for each stage of excavation.
  - d) Detail excavation depth including localized pits and sloping ground.
- 7. Adjacent building survey shall be done according to the survey form in the guideline.

## Table (2A) Allowable Wall Deflection Limits

No.	Distance	Zone	Allowable maximum wall deflection limits, $\delta_w/H$
1	H > d	Zone 1	< 0.5 % H
2	2H > d > H	Zone 2	< 0.7 % H
3	d > 2H	Zone 3	0.7 % H for ground type A
		20110 5	1.0 % H for ground type B

Where,  $\delta_w = maximum$  wall deflection

H = Excavation depth,

d = distance between existing structure and the edge of the excavation

Ground Type A = over-consolidated stiff clays and silts, residual soils, and medium to dense sands

Ground Type B = soft clays, silts or organic soils.

Allowable displacement: Near existing building with allowable displacement shall be < 0.5 H%.

#### **Geotechnical Design Requirement**

 The surcharge load shall be considered a minimum value of <u>10 kN/m</u><sup>2</sup>. Additional surcharge loading shall be used in the design to take account of incidental loading arising from adjacent buildings, working area, construction plant and stacking of materials.



## What is Geotechnical Building Works (GBW)?

Tunneling Works

Building and Construction

- Any excavation or other building works to make a tunnel with a diameter, width or height or more than 2 m
- Excavation Works and Earth Retaining Structures
  - Any <u>excavation</u>, or other building works to make a caisson, cofferdam, trench, ditch, shaft, well with a <u>depth of more than 6 m</u>
  - Any building works for constructing, altering or repairing any <u>earth</u> retaining structures in or for a trench, ditch, shaft, well with a <u>depth or</u> height or more than 6 m
  - Any earthwork or other building works for constructing or stabilising a slope with a height of more than 6 m (measured as vertical distance between the highest level to the lowest level of the slope)
- Foundation Works
  - Foundation for buildings of 30 or more storeys





## Advisory Note 1/09 on ERSS

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Key	UU		5
			-

Movement control limit

Table 1: Allowable maximum ERSS wall deflection limits

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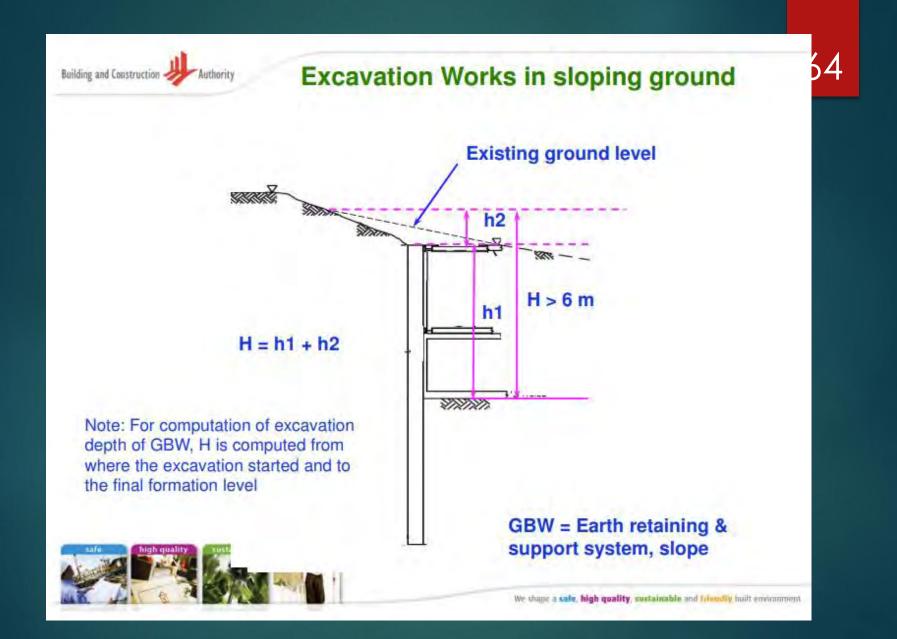
Wall deflection limits/Zones	Locations of buildings, structures and critical utilities				
where * - distance from excavation face H = excavation depth	Zone 1 (x/H < 1)	Zone 2	Zone 3 (X/H > 2)		
õ <sub>e</sub> = Wall deflection		(1 ≤ x/H ≤ 2)	Ground Type A	Ground Type B	
Allowable maximum ERSS wall deflection limits (õ <sub>w</sub> /H)	0.5%	0.7%	0,7%	1.0%	

Ground Type A refers to over consolidated still clays and silts, residual soils, and medium to dense sands; and Ground Type B refers to soll clays, silts or organic soils extending to or below formation level (e.g. Kallang Formation) and loose fills.

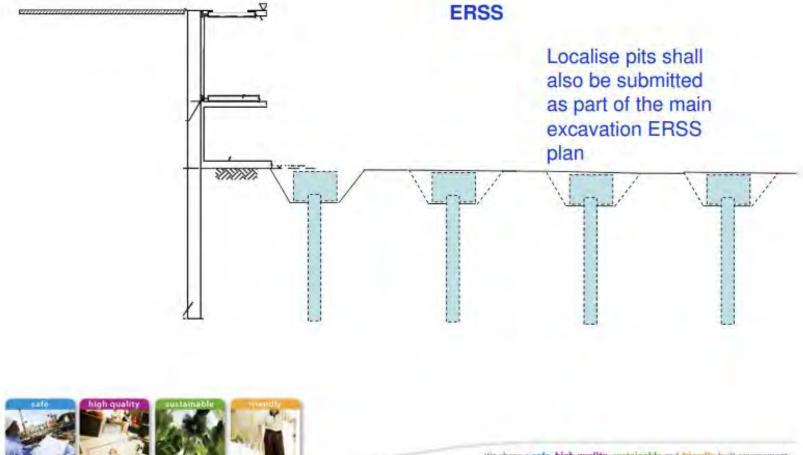
10 In any case, the allowable wall deflection limits shall also be determined by the prevention of structural damage to neighbouring buildings or structures arising from ground deformations.

#### Table 2: Control strategies guides for ERSS.

	-	Allowable limits			
	Zone	Alert level	Work	suspension level	
Critical limit		70% WSL Allowable wall deflection limit			
	No	Allowable limits			
	pu	Check level	Alert level	Work suspension level	
ALL ALL	N So S	50% WSL	70%WSL	Allowable wall deflection limit	in the built enveronm

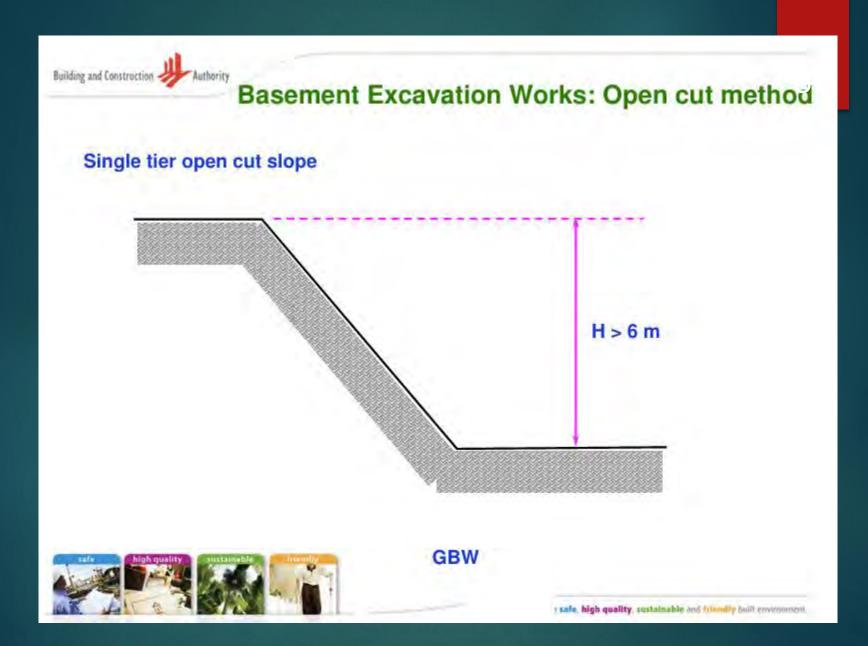


# **Excavation Works: Basement Construction**



Building and Construction -

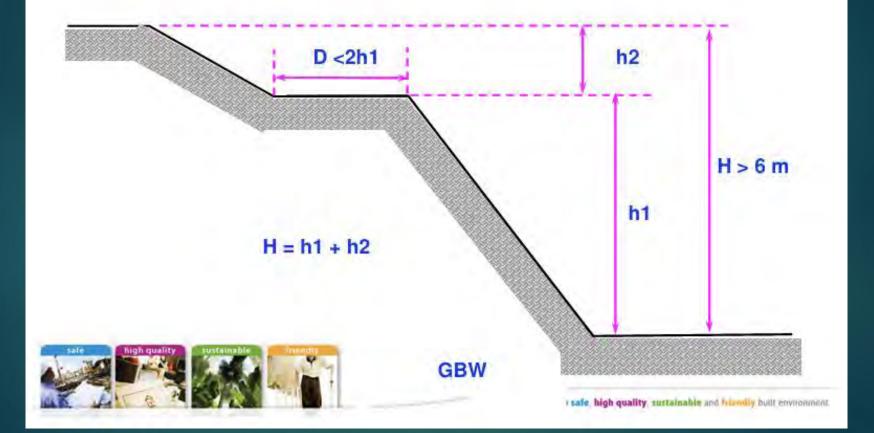
Authority

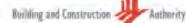




# Basement Excavation Works: Open cut method

#### Multi-tier open cut slope in stiff soils





#### Submission Requirement for ERSS

	Appointments Required		
All permanent or temporary building works that involve	Qualified Person (QP)	Accredited Checker (AC)	
Excavation/ERSS ≤ 1.5 m** deep	Plan approv	al is not required	
$1.5 \text{ m}^{**} < \text{Excavation/ERSS} \le 4 \text{ m deep}$	QP(ST)	AC is not required	
$4 \text{ m} < \text{Excavation/ERSS} \le 6 \text{ m} \text{ deep}$	QP(ST)	AC	
Excavation/ERSS > 6 m deep and not classified as Geotechnical Building Works (GBW): e.g. excavation for sewer manhole associated with pipe diameter of 2 m or less	QP(ST)	AC	
Excavation/ERSS > 6 m deep and classified as GBW. E.g. basement excavation.	QP(ST) QP(Geo)	AC AC(Geo)	

Notes:

Plan approval is not required for insignificant building works listed on First Schedule of Building Regulation 3A.

\*\* If the structure that retains earth is not constructed of reinforced concrete or steel, then the applicable depth is 1 m instead of 1.5 m.

Planning approval is no longer required for any retaining wall or earth-retaining structure for supporting the face of an excavation made for the purpose of constructing any pile cap, footing, sump, lift pit or trench, provided that the size of these structures does not exceed 10 square meters in area and 2 meters in depth.

## Re-used of structural steel material



Building and Construction



Engineer to specify specification of steel material on plan and check the condition of steel material at site.

Where re-used structural steel is used, the structural design shall fully consider any imperfections and conditions of such materials

Quality assurance scheme developed for "reused struts" for bracing excavations has been incorporated into the BC1:2012.

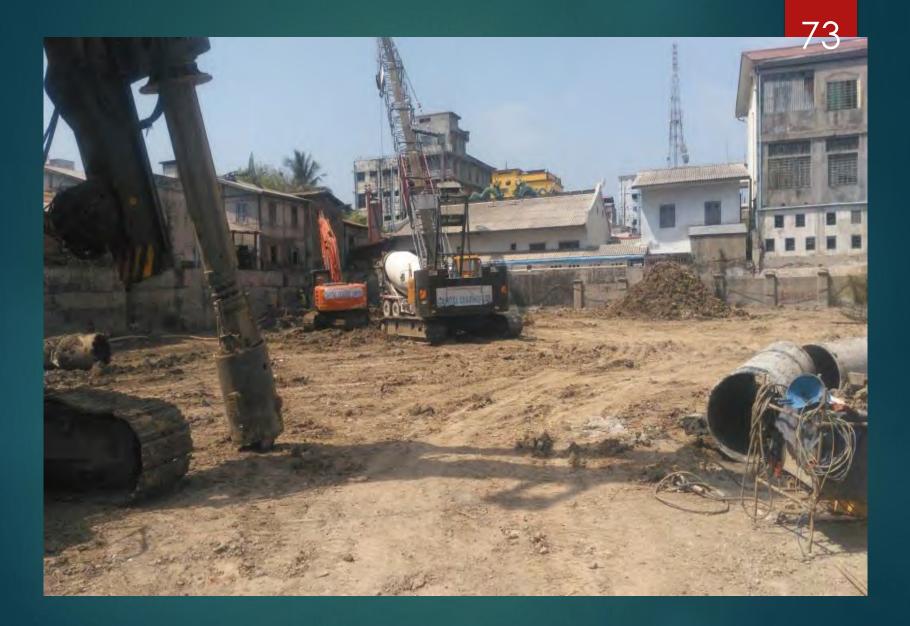


# INTERVAL

How to Access/ Interpret Instrumentation & Monitoring Data & Report (Case Study)

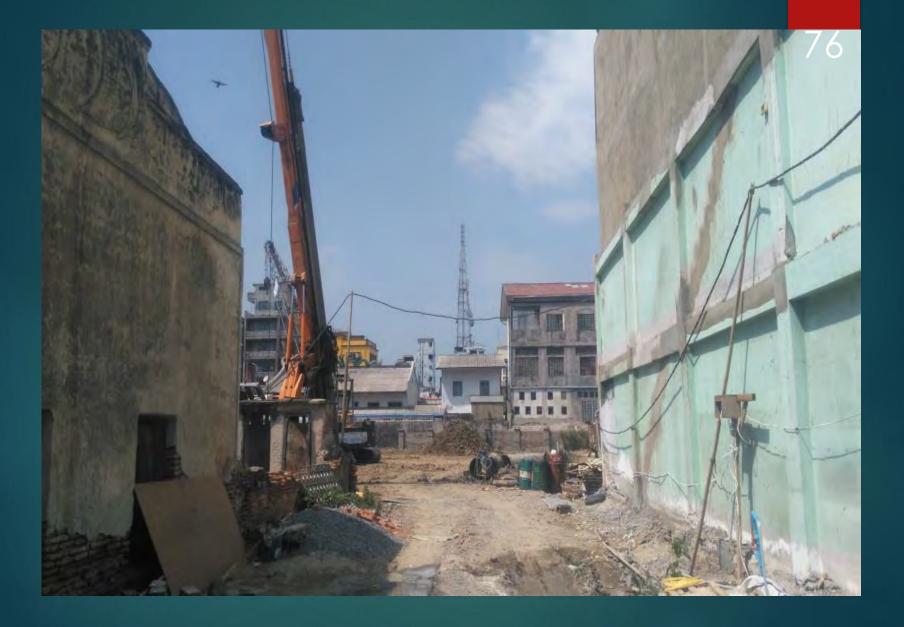
## CAPITAL CENTRE PROJECT 26-STOREY WITH 2-BASEMENT

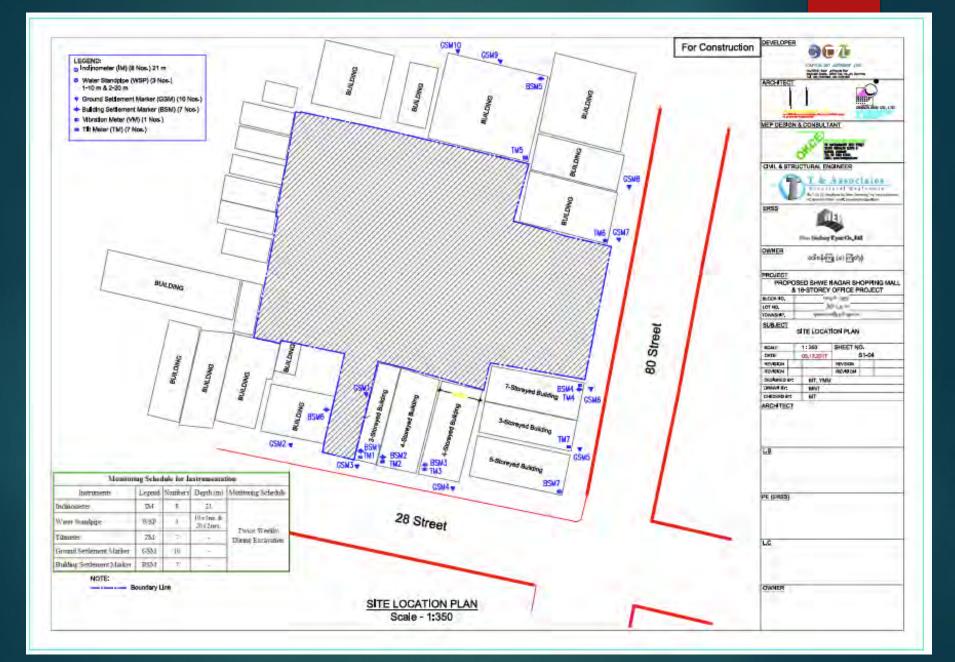


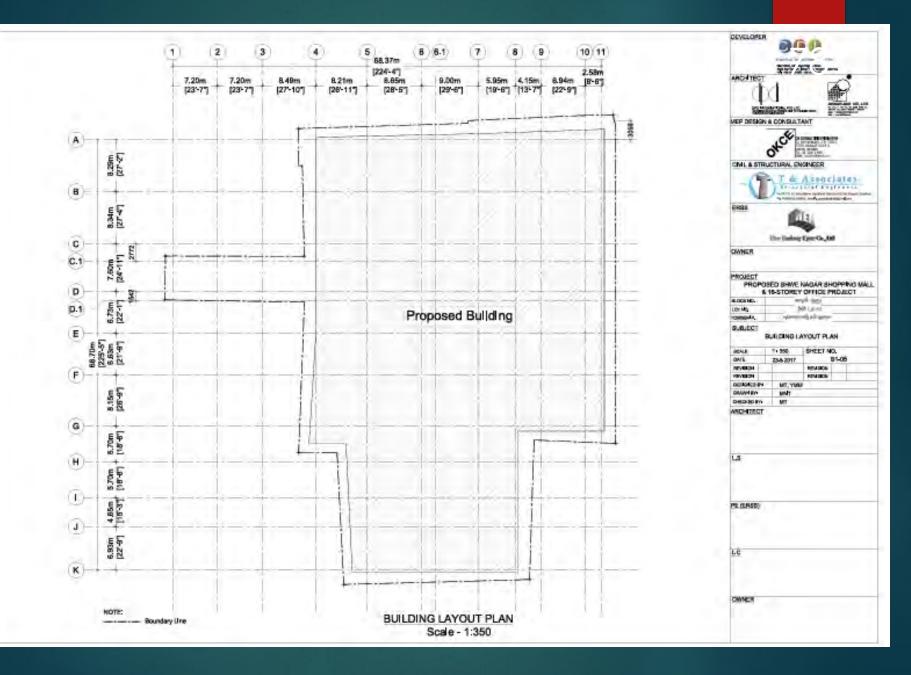


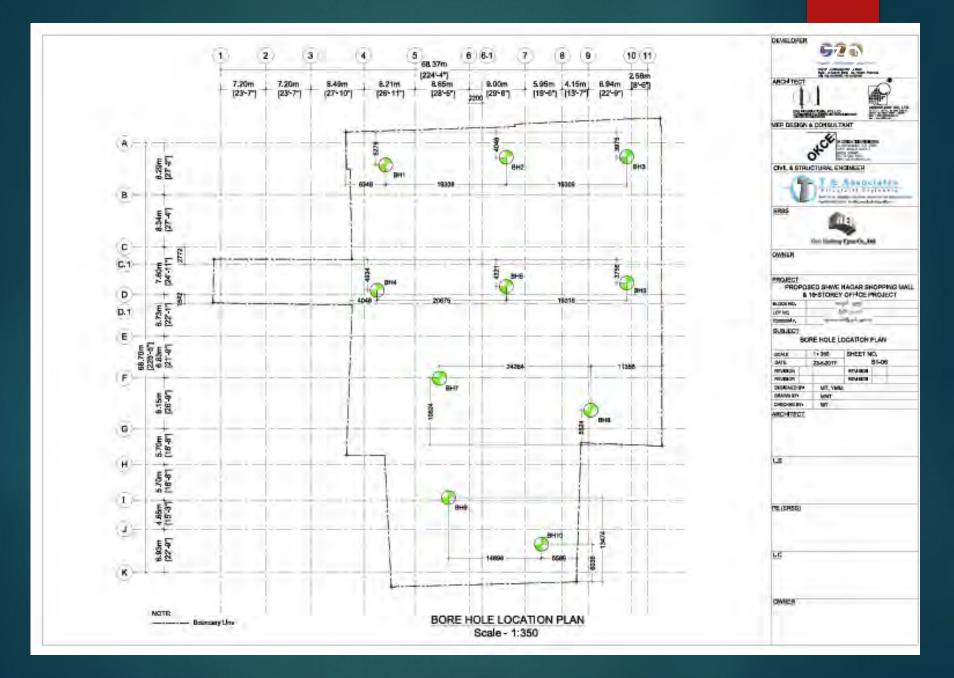


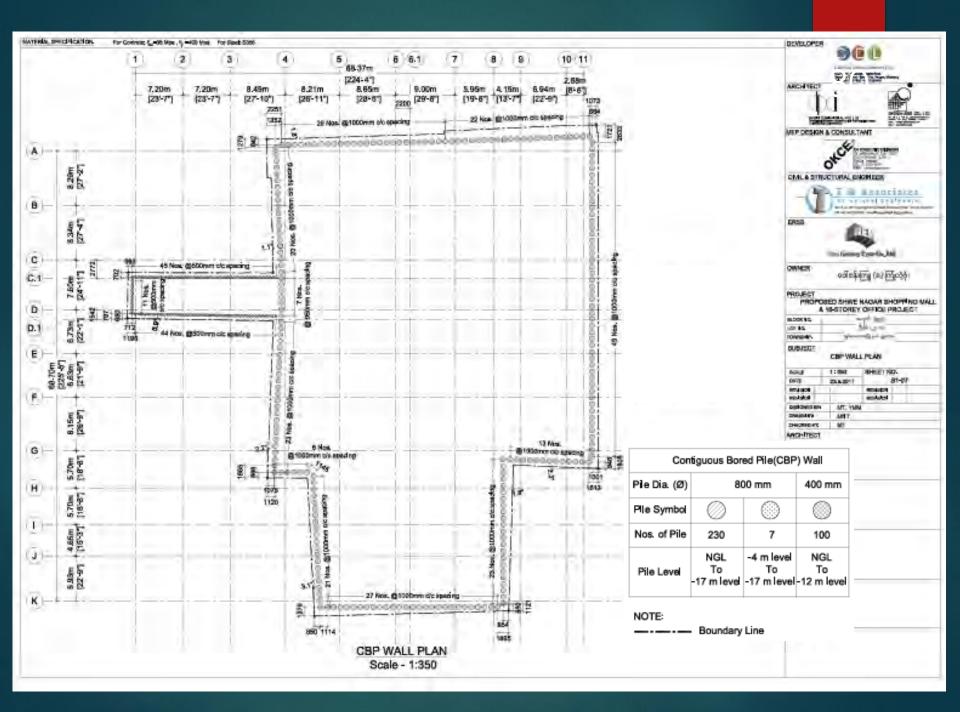


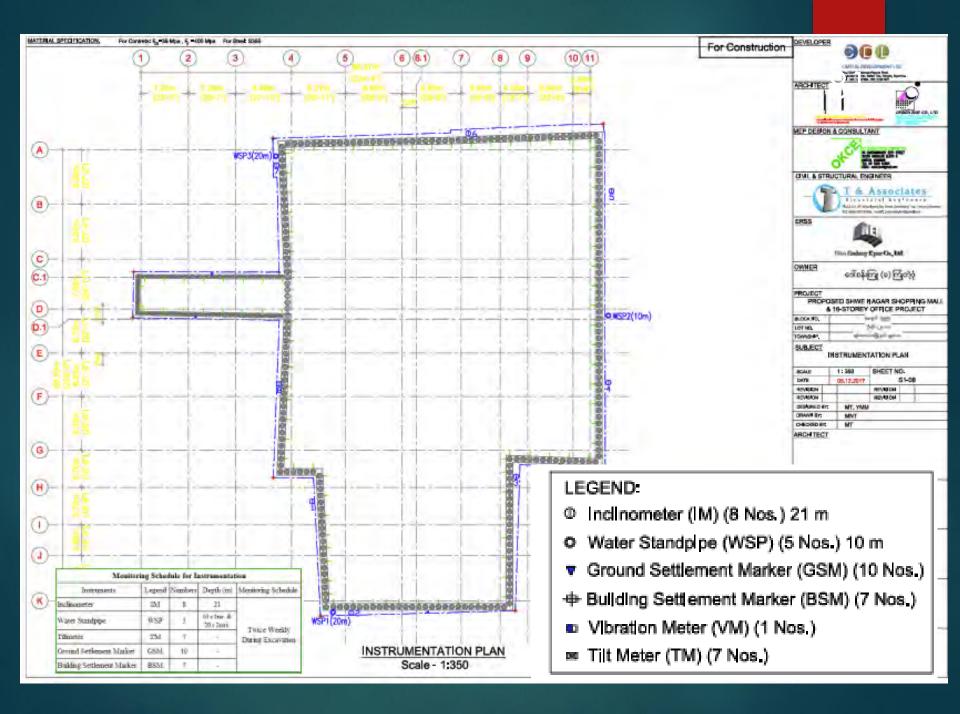








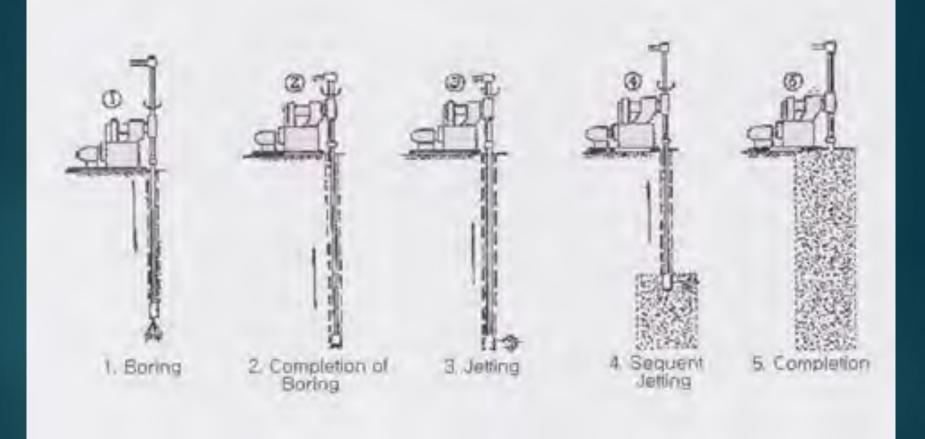




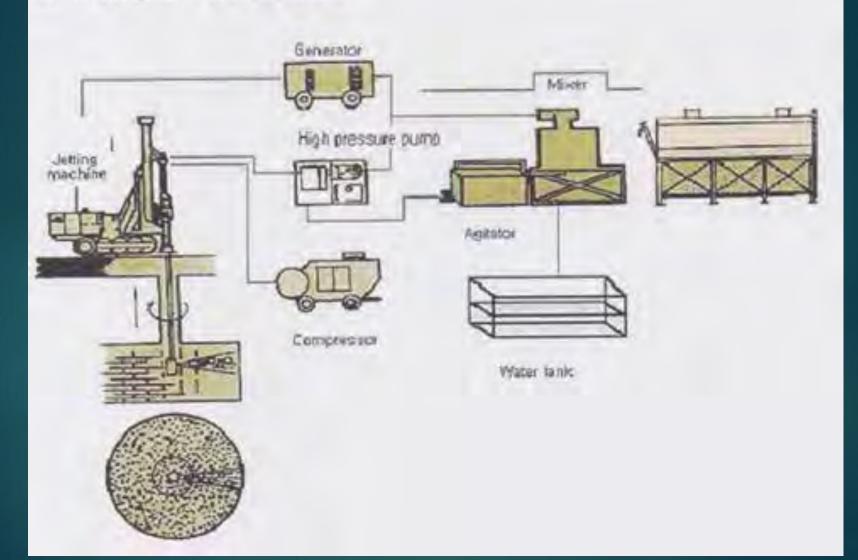
## JET GROUT BETWEEN BORED PILES TO SEAL OFF CBP







## 5.3. Arrangement of Equipments



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## 6. Grouting Materials & Their Mixing Ratios

6.1. Cement : Portland Cement Type I, in conformance with ASTM C150, packaging in a 50 kg/bag

Water : Clear Water from Site Location

Admixture : Water Reducing Admixture, Conmix Brand - SPIC

Intraplast : ZX (Extra Expanding Grout Admixture)

SHWE NAGAR SHOPPING MALL PROJECT

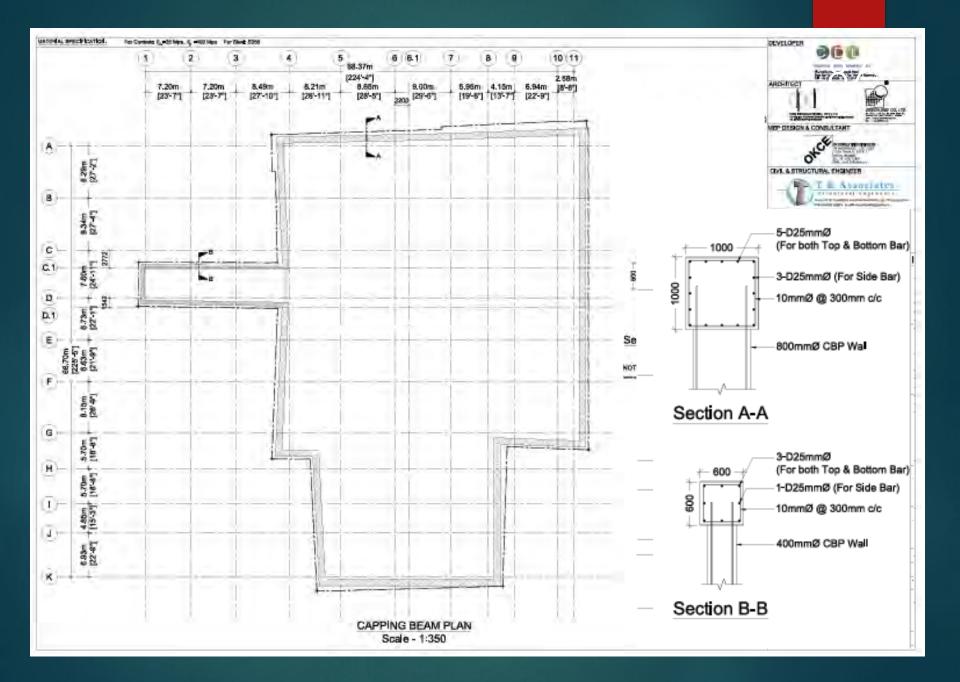
JET GROUTING CONSTRUCTION

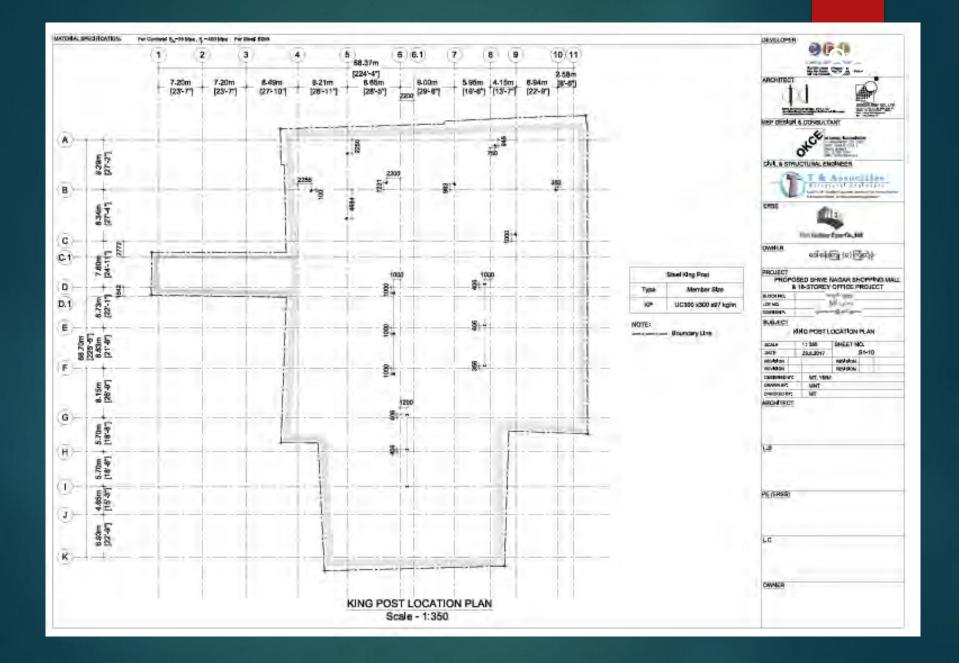
Mix No.	Grout Mix Ratio (By Weight)	Type of Grout
SCG-SP1C-ZX-01	W:C:A:ZX = 1 : 1 : 0.005 : 0.005	Jet Grouting
SCG-SP1C-ZX-02	W:C:A:ZX = 0.7 : 1 : 0.005 : 0.005	Jet Grouting

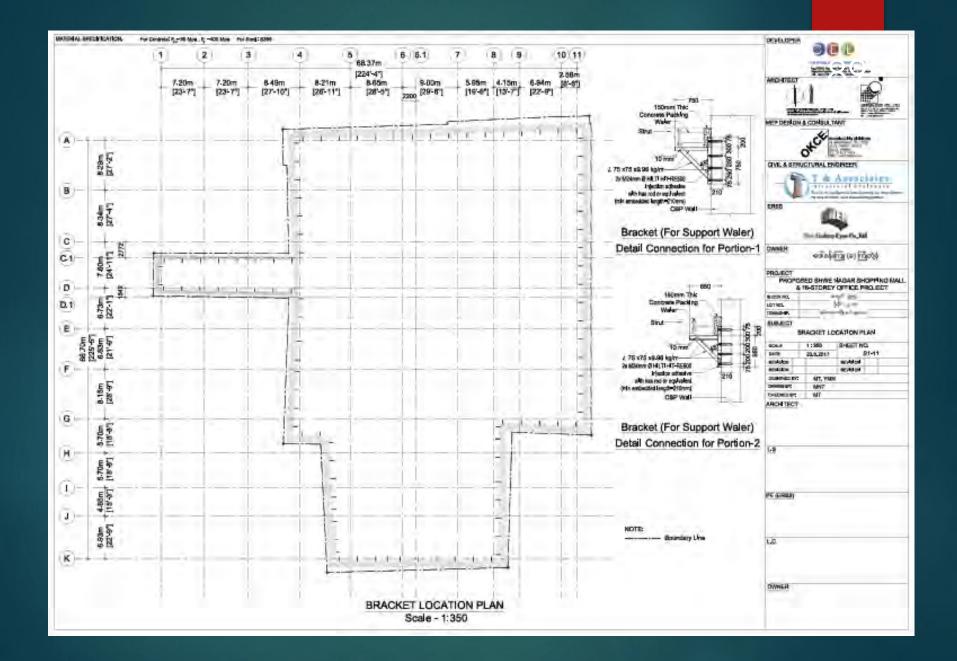
### 7. Jetting

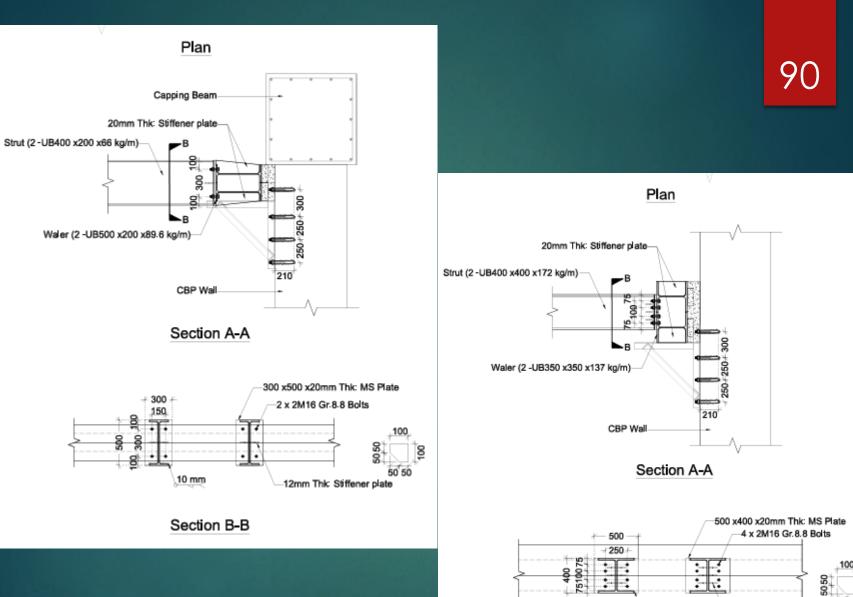
- After completion of Boring up to 17.00m, operating mode will be converted 'boring mode' to 'jetting mode'.
- 7.2. Injection pressure shall be increased to the designed, 50kg/cm2 and or 200kg/cm2 gradually. After that, jetting will be set to. In this project, planned injection system is as follows :

	Double Tube Jet Injection (Diameter of Nozzle: 2.3 - 4 mm)
Injection Pressure: 50Kg/cm <sup>2</sup>	<ul> <li>□ Classification of PUMP : YBM SG-30SV</li> <li>□ Extracting Length of 1 Step : 5 cm ( 20 Step / Imeter )</li> <li>□ Jetting Time for 1 Step : Designed Quantity 354Kg/m→7.5sec</li> <li>□ Flow rate per minute : 180 U/min ± 10 U/min</li> <li>□ r.p.m : 45 rpm ~ 75 rpm</li> </ul>









Section B-B

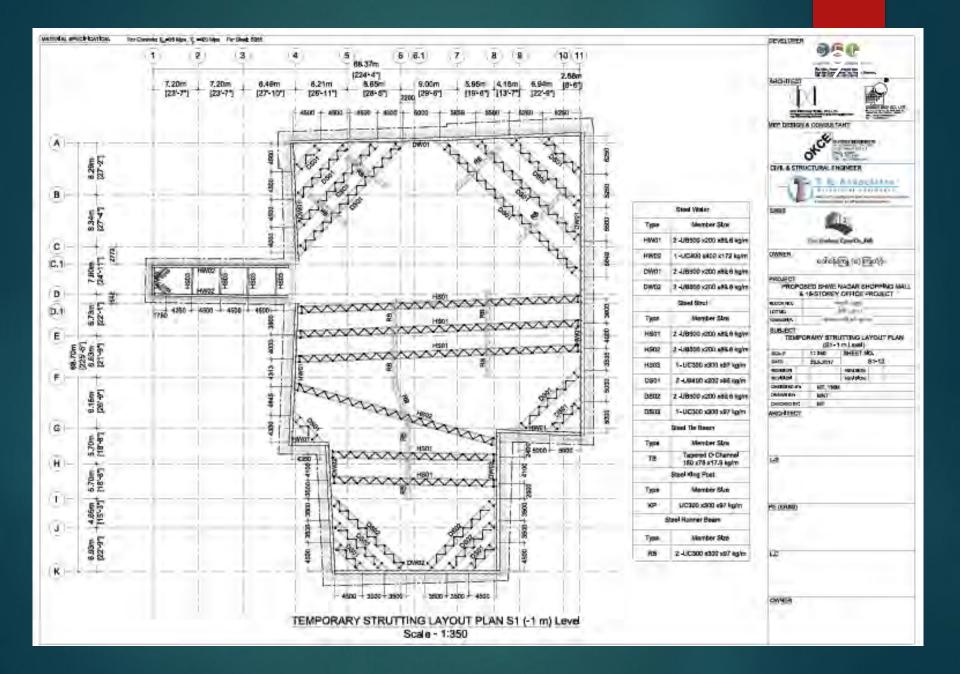
10 mm

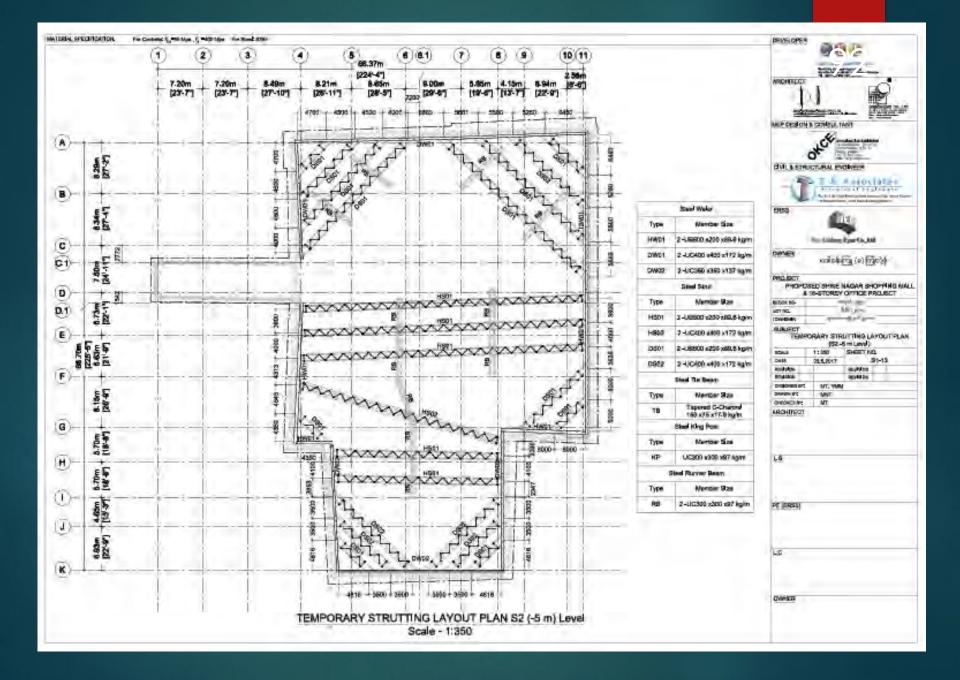
à

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50 50

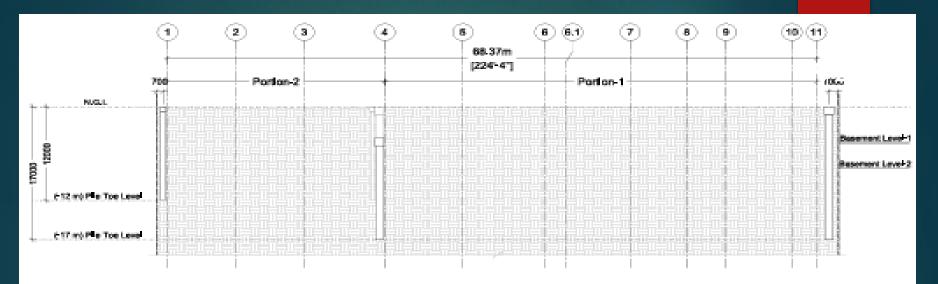
12mm Thk: Stiffener plate



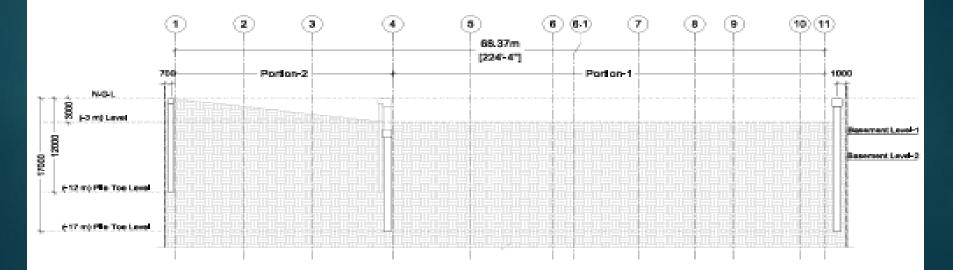


93

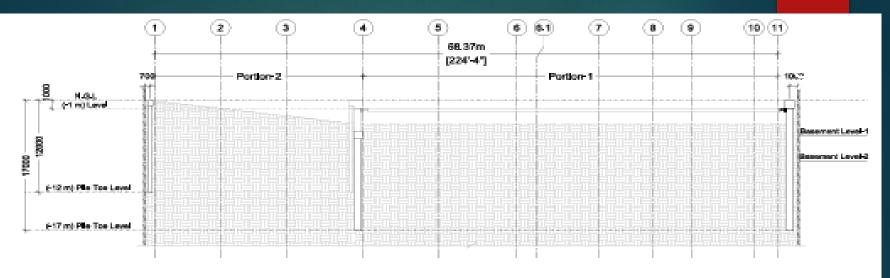
## CONSTRUCTION SEQUENCE FOR DEEP EXCAVATION



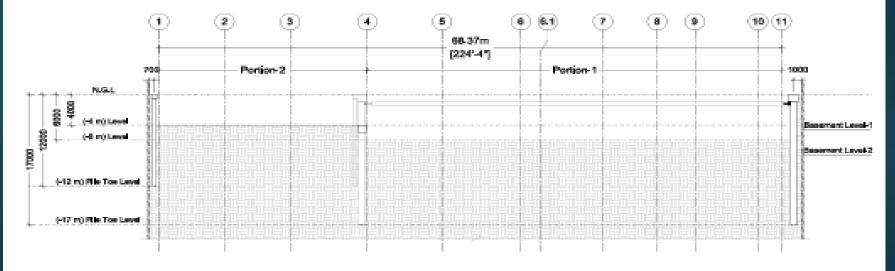
Stage 1 - Install CBP Wall and capping beam for Portion-1 & Porion-2.



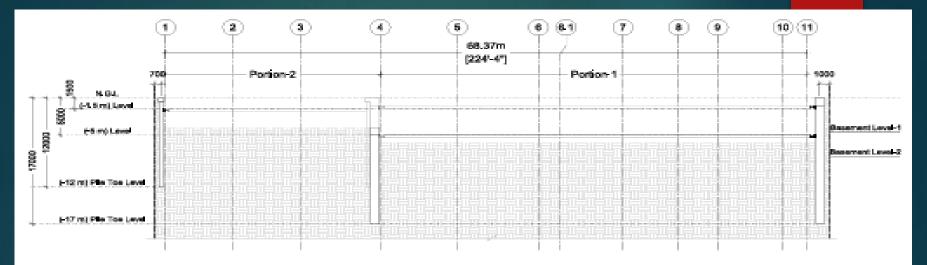
Stage 2 - Excavate upto (-3 m) Level Below N G L

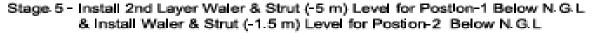


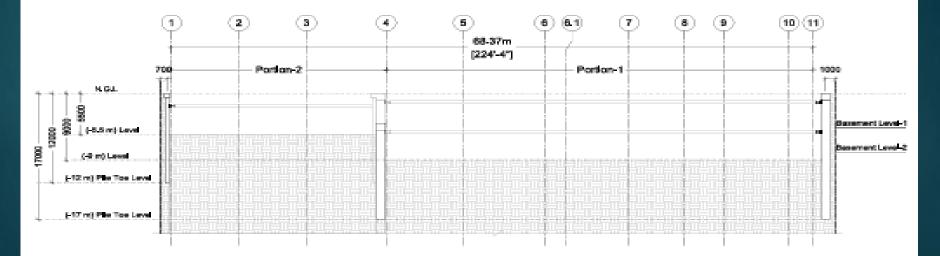
Stage 3 - Install 1st Layer Waler & Strut (-1 m) Level for Postion-1 Below N.G.L.



Stage 4 - Excavate upto (-6 m) Level for Poston-1 Below N.G.L & Excavate upto (-4 m) Level for Poston-2 Below N.G.L



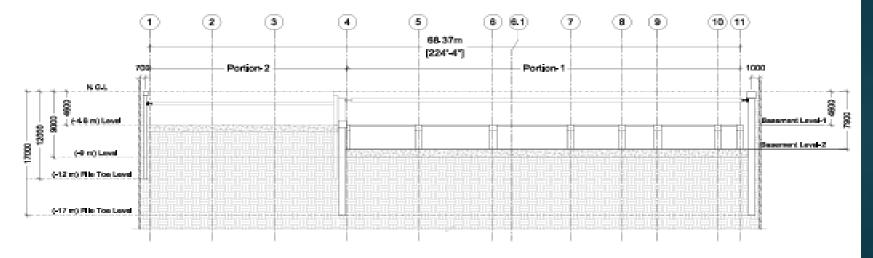




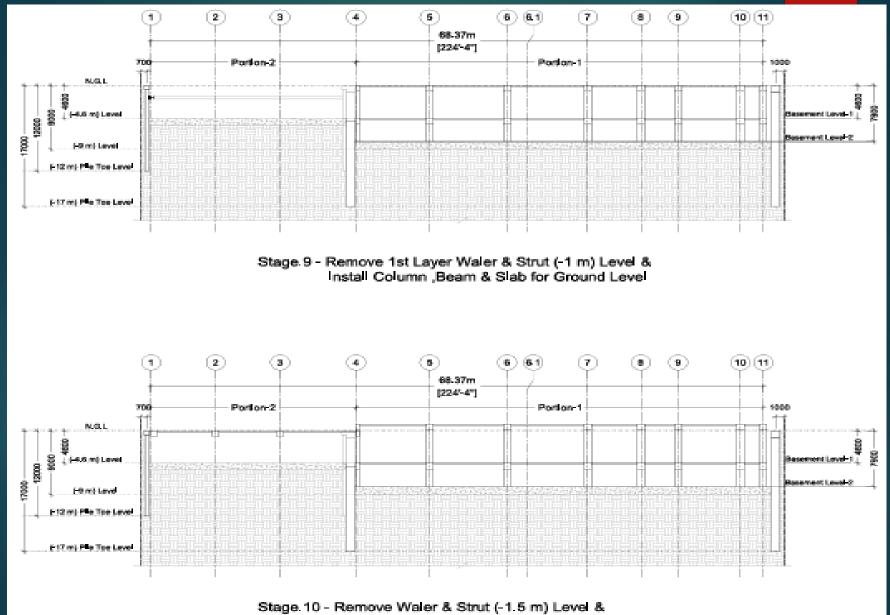
Stage 6 - Excavate upto (-9 m) Level for Postion-1 Below N.G.L & Excavate upto (-5.5 m) Level for Postion-2 Below N.G.L



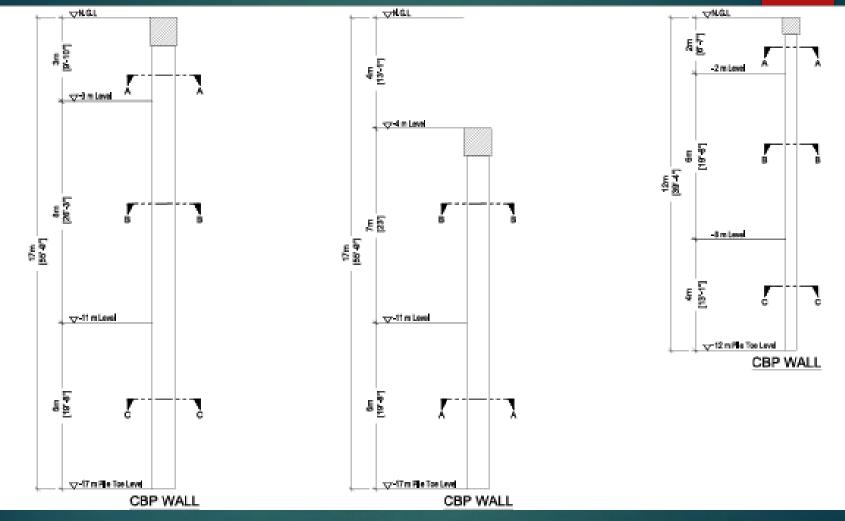
Stage 7 - Cast Footing for Basement-2 (-7.9m) Level for Postion-1 & (-4.6m) Level for Postion-2



Stage 8 - Remove 2nd Layer Waler & Strut (-5 m) Level & Install Column ,Beam & Slab (-4.6m) Basement Level-1 for Postion-1



Install Column ,Beam & Slab for Ground Level





#### Inclinometer Monitoring Results

roject G ate of Installe educed Level	d :25/1/20	018	ion for Shwe Nag	ar Project	Instrument M Date of Initia Date of Moni	: IM-4 : 29/1/2018 : 16/11/2018	
Depth (m)	AØ	A180	D (mm)	BO	B180	D (mm)	Res D (mm)
0.5	111	-147	4.04	853	-818	3.54	5.37
1.0	191	-234	-3.00	757	-746	1.22	3.24
1.5	204	-247	-3.15	735	-739	0.24	3.16
2.0	250	-293	1.90	769	-755	-0.22	- 1.91
2.5	295	-337	-1.53	726	-721	-1.39	2.07
3.0	287	-325	-1.90	643	-650	-0.42	1.95
3.5	187	-231	-1.95	597	-593	-0.18	1.96
4.0	150	-186	-2.06	587	-591	-0.61	2.15
4,5	143	-183	2.07	644	-629	-0.77	2.21
5.0	155	-193	-1.60	696	-696	-0.76	1.77
5,5	119	-155	-1.49	765	-761	-0,57	1.60
6.0	152	-187	-0.57	736	-743	-0.28	0.64
6.5	169	-201	-0.28	625	-640	-0.31	0.42
7,0	217	-261	1.11	591	-580	0.71	1.32
7.5	216	-253	0.95	669	-655	-0.24	0.58
9.0	216	-256	0.78	688	-690	-0.07	0.78
8.5	205	-245	1.57	666	-663	-0.20	1,58
9.0	193	-224	2.37	624	-626	-0.16	2.38
9.5	208	-249	2.24	576	-597	-0.47	2.29
10.0	200	-241	2.36	527	- 522	-0.38	2.39
10.5	259	-303	2.53	565	-598	-0,17	2.54
11.0	315	-361	2.95	473	-490	-0.21	- 2.96
11.5	327	-360	2.18	449	-455	-0.48	2.23
12,0	431	476	2.20	\$57	- 575	-0.41	2,24
12.5	418	-455	2.28	662	-672	0.43	2.32
13.0	331	-365	1.63	667	-660	-0,15	1,64
13.5	242	-272	1,56	679	-676	0.00	1.56
14.0	263	-292	1.29	628	-635	-0.18	1.30
14.5	414	449	0.95	573	-597	-1.17	1.51
15.0	276	-302	1.12	788	-810	1.17	1.62
155	116	-161	0.47	525	537	-0.24	0.53
16.0	162	-226	0.63	581	-584	-0.18	0.66
16.5	175	-219	0.41	583	-577	0.03	0.41
17,0	200	-242	0.13	540	- 537	-0.05	0,14
17.5	247	-297	0.14	596	-605	-0.17	0.22
18.0	249	-286	0.22	610	-608	-0.06	0.23
18.5	198	-241	0.27	- 539 -	-535	0.22	0.35
19.0	58	-97	0.27	414	-414	0.00	0.27
19.5	-19	-29	0.17	374	370	0.02	0.17
20.0	-44	-4-	0.15	343	- 322	-0.01	0.15
the second se							

0.25

9

301

-292

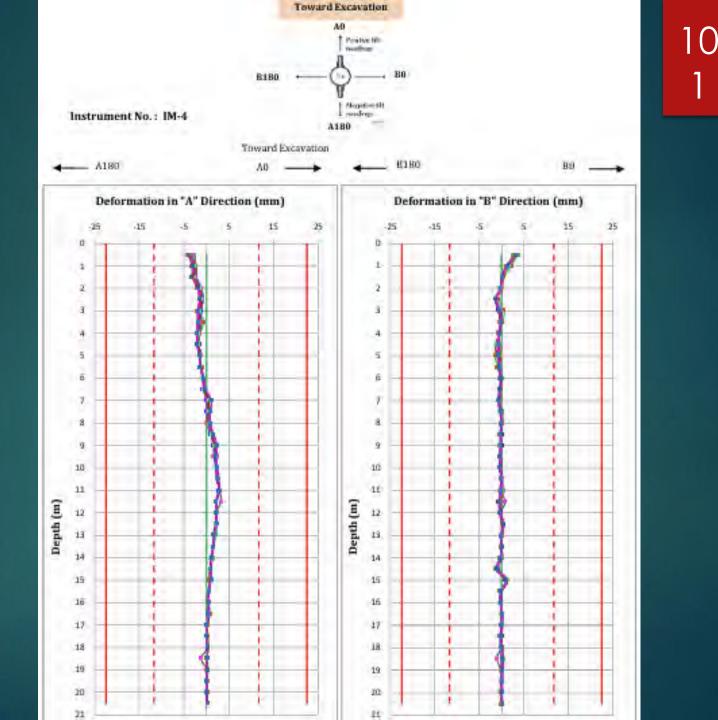
0.15

0.29

20.5

-50

## 10 0



#### WATER LEVEL MONITORING RECORD SHEET



GEO-FRIENDS

CLIENT	: Capital Development Ltd.
PROJECT	: Geotechnical Instrumentation for Shwe Nagar Project
LOCATION	: 80th Street, Between 27th & 28th Street, Manda by

INSTRUMENT NO.	: WSP-1
INSTALLED DATE	: 4 12.2017
LENGTH OF WATER STANDPIPE	: 20.00 m
PIPE ABOVE GROUND LEVEL	: 0.15 m

		11 - 11	ELAPSED	WSP	1			
DATE	TIME	INTERVAL (day)	TIME (day)	WATER TABLE LEVEL Below Ground Level(m)	CUMULATIVE CHANGE(m)	REMARK		
07-Feb-18	7:58	đ	a	8.490	0.000	Initial Reading		
22-Sep-18	10:00	1	227	8.830	0,340	Sam Reading		
23-Sep-18	9:15	1	2.28	8.850	0.360	59th Reading		
24-Sep-18	9:27		229	06.8.8	0340	60m Reading		
25-Sep-18	9:35	1	230	8.780	0,290	6 1st Reading		
27-Oct-18	13:20	32	262	8.520	0,030	62nd Reading		
29-0:3-18	8:52	2	264	8,500	0.010	63rd Reading		
02-140-18	10:40	4	268	8.540	0.050	64th Reading		
05-Min+18	9:45	3	271	8.540	0.050	65m Reading		
09-Nov-18	10:05	4	275	8.560	0.070	668) Reading		
12-Nov-18	9:30	3	278	8.550	0.060	67th Reading		
16-140-18	9:11	4	282	8.540	0,050	69uy Reading		
						-		
						€		
-	_							
-		1 1				* <u>-</u>		

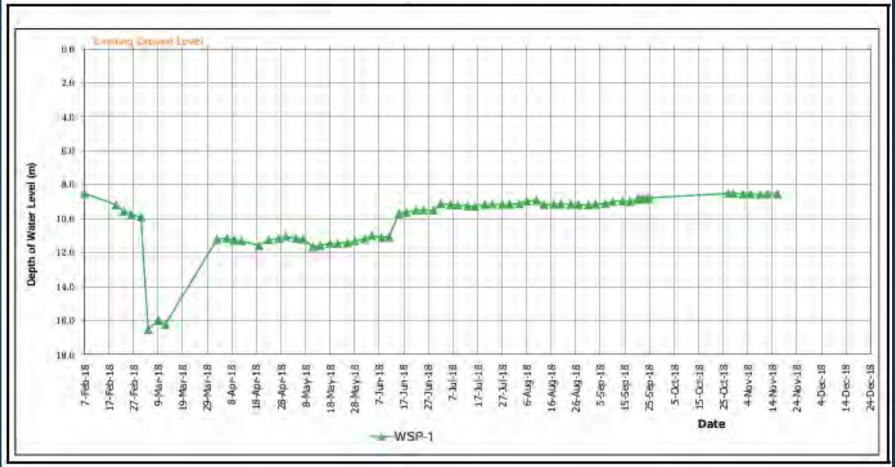
#### WATER LEVEL MONITORING RECORD SHEET



#### GEO-FRIENDS

Engineering & Construction Do., Ltd.







- CLIENT Capital Development Ltd.
- PROJECT Gestednical Instrumentation for Shive Nagar Project
- LOCATION

81 + 0.115 deg (1/900)

WSL = 0.181 deg (1/300)

80th Street, Botween 27th & 28th Street, Mandalay

#### TILTMETER MONITORING RESULTS

INSTUMENT NO	1111
INSTALLED DATE	29-Jan 18
INITIAL DATE	20-548-18

20-Feb-18			3	CHANGE	(Deg)	(Deg, Min, Sec)	
	0	-32	107	0	0.0000	00'00'00	0
14-540-18	206	-20	99	10	6.0229	00'01'23'	1/2500
17-Sep-18	209	-22	98	19	0,0218	co.07,18,	1/2632
18-5ep-18	210	-17	92	30	0,0344	00/02/04*	1/1667
20-Sap-18	212	-21	95	23	0.0264	00'01'35'	1/2374
21-5ap-18	213	-19	97	23	0.0264	00'01'35'	1/2374
22-Sep 18	214	22	92	40	0.0229	00'03'23'	1/2500
23-5ep-18	215	-20	95	24	0,0775	00.01.38.	1/2084
24-Sep-88	215	-20	94	25	0.0286	00'01'43'	1/2000
25-Srp-18	217	91-	95	25	0.0286	00'01/43"	1/2000
17-Get-18	249	-22	92	20	0.0229	00/01/23*	1/2500
29-011-18	251	-18	97	24	0.0275	00*05*39*	1/2084
2-Nov-18	255	-45	95	29	0,0332	00/02/00	1/1725
5-Nov-18	258	-17	97	25	0,0286	00'01'43'	1/2000
9 Nov-18	262	-15	96	28	0.0321	00'01'56"	1/1786
12-904-18	265	-42	94	33	0.0378	00/02/16	1/1516
18-409-18	269	-10	35	34	6.0390	00102120	1/1471

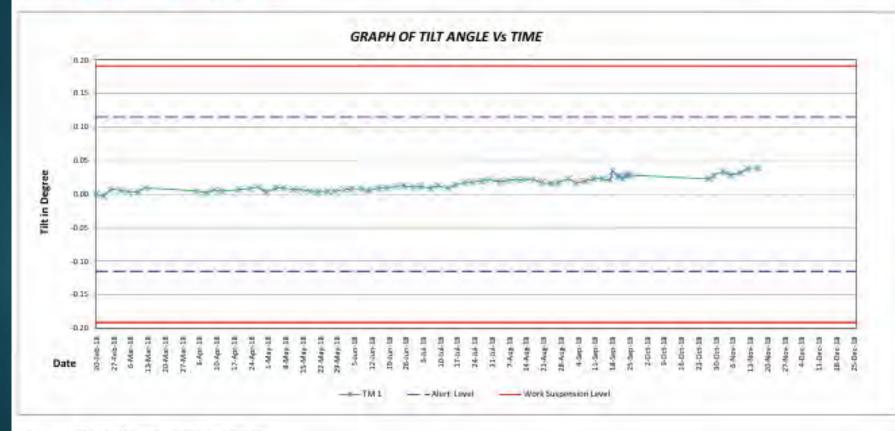
Note: > Tit - Tilting Forward relative to base reading

- Tilt - Tilting Backward relative to base reading



#### **Tiltmeter Monitoring Results**

CLIENT -	Capital Development Ltd.	INSTUMENT NO	TM 1
PROJECT -	Geotechnical Instrumentation for Shive Nagar Project	INSTALLED DATE -	29-Jan-18
LOCATION -	80th Street, Between 27th & 28th Street, Mandalay	INITIAL DATE	20-Feb-18
AL + 0 115 4x4 (1/500)	(8)5 + 0 501 6++ (1/200)		



Note: + Tilt - Tilting Forward relative to base reading

- Tilt = Tilting Backward relative to base reading

620		O-FR				Ground Settlement Marker Monitoring Results							
Client :	Capital Develop	pment Ltd.											
Project :	Geotechnical Instrumentation for Shwe Nagar Project												
Location :	80th Street, Between 27th & 28th Street, Mandalay Installed Date : 26/1/2018												
Survey Date	31-Jan-18	02-Nov-18	05-Nov-18	09-Nov-18	12-Nov-18	16-Nov-18				Diff from	Diff from		
Point No.	Initial Reading (m)	64th Reading (m)	65th Reading (m)	66th Reading (m)	67th Reading (m)	68th Reading (m)	69th Reading (m)	70th Reading (m)	71st Reading (m)	Previous (num)	Initial (mm)		
GSM 1	99.938	99.940	99.940	99.940	99.941	99.939	-			2	1		
GSM 2	99.800	99.794	99,795	99,796	99.795	99.795				0	-5		
GSM 3	99.807	99,802	99.802	99,801	99.802	99.801				-1	-6		
GSM 4	99.918	99.919	99.918	99.917	99.918	99.918				a	ũ		
GSM 5	99.880	99.882	99.883	99.884	99.882	99,882				U	ź		
GSM 6	99.879	99.879	99.880	99.879	99.879	99.878				>1	-1		
GSM 7	99.770	99.764	99.765	99:764	99.764	99.765				1	-5		
GSM 8	99.770	99.769	99.770	99.769	99.768	99.768				ñ	-2		
GSM 9	101.102	101.101	101.100	101.099	101.100	101.100				A	-2		
GSM 10	100.677	100.676	100.676	100.675	100.677	100.676				-1	-1		

Note: 1 (-) Sign is Settled (+) Sign is Heaved

\* Reference RL value - Assumed 100m

Aleri Level = 17.50 mm Preservation 1 and - 21,20 mm

Work Suspension Level - 25.00 mm

Remark: GSM 1 was reinstalled and reinitialized

Installed Date : 26/1/2018

Predetermine Level - 21.30 mm

Alert Level = 17.50 mm

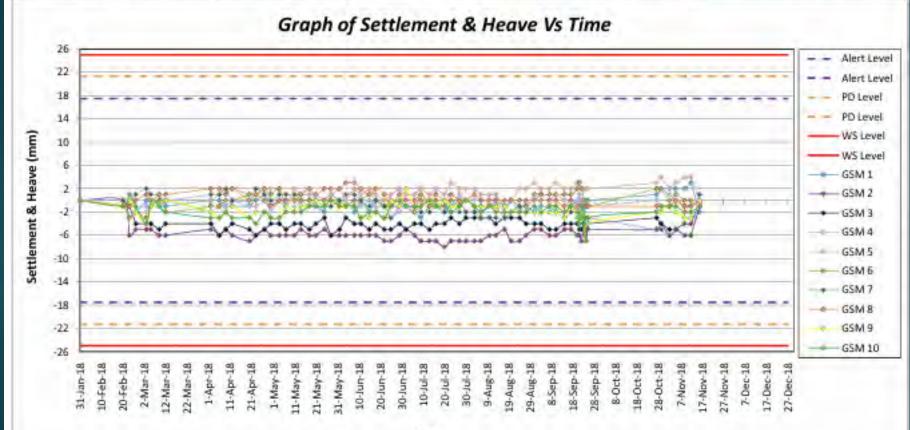
Work Suspension Level - 25.00 mm



Client : Capital Development Ltd.

Project : Geotechnical Instrumentation for Shwe Nagar Project

Location : 80th Street, Between 27th & 28th Street, Mandalay



Date

		O-FR				Building Settlement Marker Monitoring Results						
Client :	Capital Develop	pment Ltd.				_						
Project :	Geotechnical Instrumentation for Shwe Nagar Project											
Location :	80th Street, Bet	tween 27th &	28th Street, N		Installed Date	e : 27/1/2018 &	& 28/1/2016	\$				
Survey Date	.31-Jan-18	02-Nov-18	05-Nov-18	09 Nov 18	12-Nov-18	16-Nov-18				Diff from	Diff from	
Point No.	Initial Reading (m)	64th Reading (m)	65th Reading (m)	66th Reading (m)	67th Reading (m)	68th Reading (m)	69th Reading (m)	70th Reading (m)	71st Reading (m)	Previous (num)	Initial (mm)	
BSM 1	101.180	101.179	101.178	101,178	101.179	101.180				1	0	
BSM 2	101.281	101.273	101.274	101.273	101.274	101.275				1	-6	
BSM 3	101.210	101.212	101.211	101.213	101.211	101.214				à.	đ.,	
BSM 4	100.898	100.895	100.895	100.897	100.895	100,895				6	-3	
BSM 5	101.789	101.789	101.790	101.787	101.789	101.787				-8	-2	
BSM 6	100.560	100.560	100.558	100.559	100.558	100.558				0	-2	
BSM 7	101.057	101.056	101.056	101.058	101.056	101.057			1	1	0	

Note: \* (-) Sign is Settled (+) Sign is Heaved

Aleri Level - 10.50 mm Pretievermine Level - 12.71 mm

\* Reference RL value - Assumed 100m

Work Suspension Level = 15.00 mm



Client : Capital Development Ltd.

Installed Date : 26/1/2018

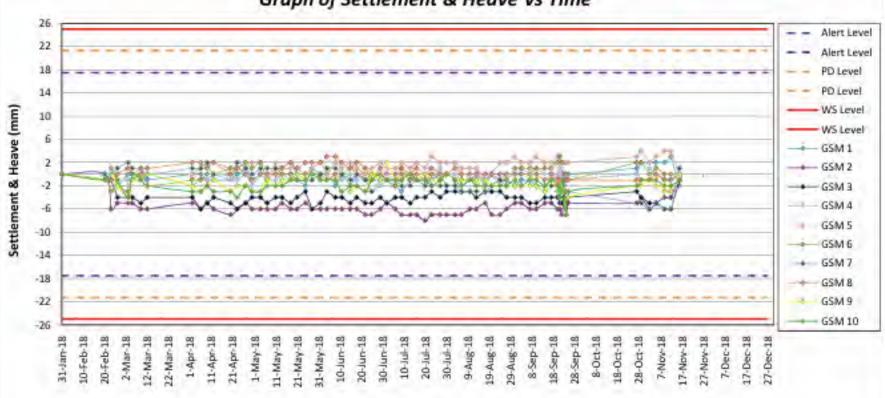
Alert Level - 17.50 mm

Project : Geotechnical Instrumentation for Shwe Nagar Project

Location : 80th Street, Between 27th & 28th Street, Mandalay

Work Suspension Level = 25.00 mm

Predetermine Level = 21,30 mm



### Graph of Settlement & Heave Vs Time

# Don't skim on instrumentation. **Penny wise dollar foolish!**

11 1

# THANK YOU! & DISCUSSION.